

Non-linear Soil Amplification for Horizontal GM



Ronnie Kamai

rkamai@berkeley.edu

NGA-West2 workshop, UC Berkeley, Nov 15th, 2012

Background

- Update to Walling et. al. 2008
- Simulation-based model to describe non-linearity in site response
 - RVT-based, 1D site response method (RASCALS)
 - Combines point-source stochastic for source with equivalent-linear for site response
 - 11 values of PGA - 0.01 through 1.5 g
 - Four models for describing soil properties (G/G_{max} , damping curves)
 - Reference velocity for amplification factors: $V_{s30}=1170$ m/s
 - 30 randomizations of profile depth, soil properties, etc.

Motivation

- Simulation database expanded and updated
 - Includes M5, M6, M7
 - Includes Vs30 as low as 190 m/s
- Explore Sa(T) vs. PGA as shaking input parameter
 - Increase ease of application for hazard analyst
 - Other studies have shown Sa(T) works well (e.g. Bazzurro&Cornell 2004, Chiou and Youngs 2008)

Range of simulation results used for model development

V_{s30} (m/sec)	<i>Depth to top of rock</i> ($V_{s30}=1$ Km/sec)	<i>Material Model</i> <i>used for</i> <i>nonlinear</i> <i>properties</i>
190	9-305 m	PR
270	9-305 m	PR, EPRI
400	9-305 m	PR, EPRI
560	9-305 m	PR, EPRI
760	79 m	PR, EPRI
900	79 m	PR

Functional form

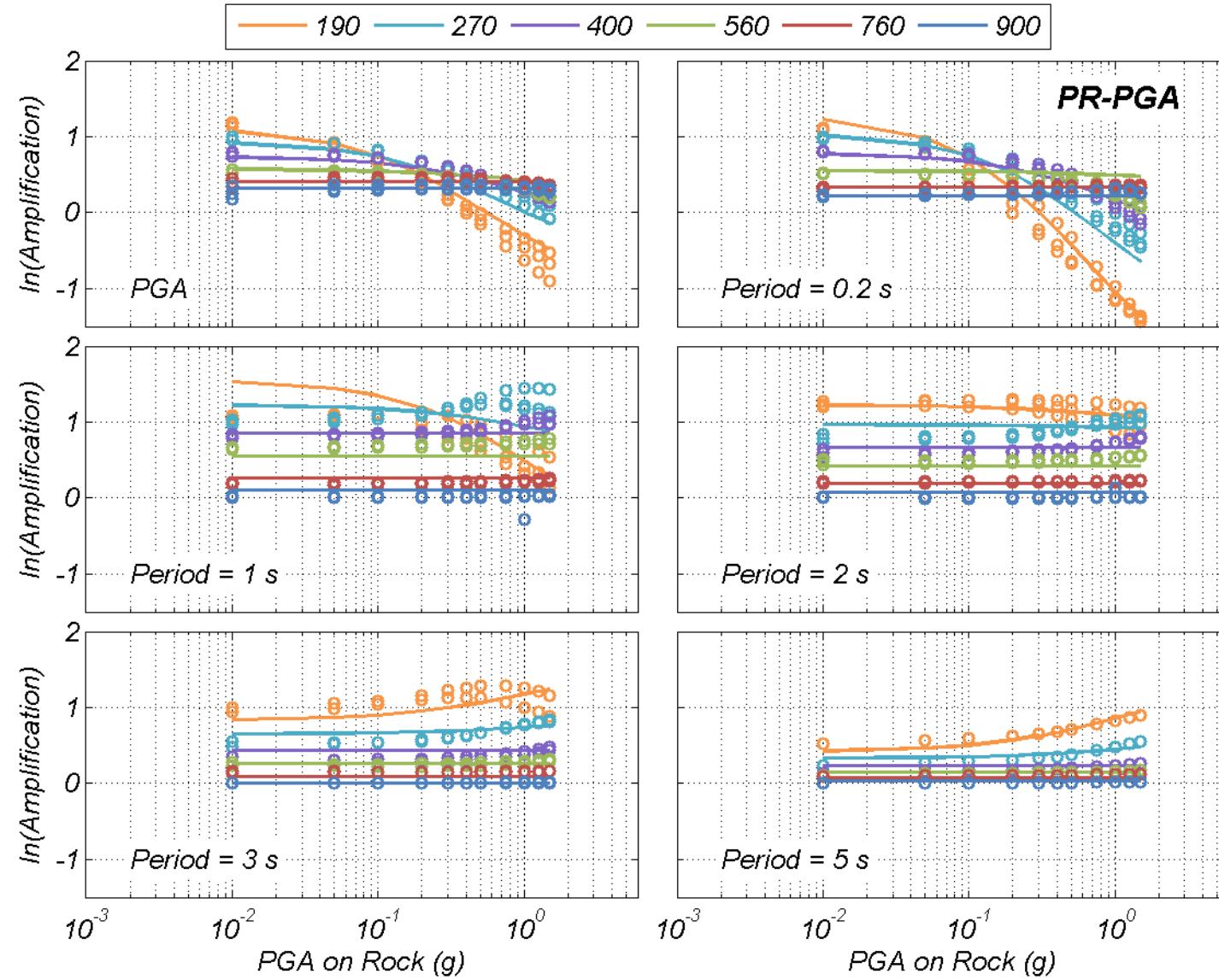
$$\ln(Amp) = f_L(V_{s30}) + f_{NL}(GM_{Rock}, V_{s30})$$

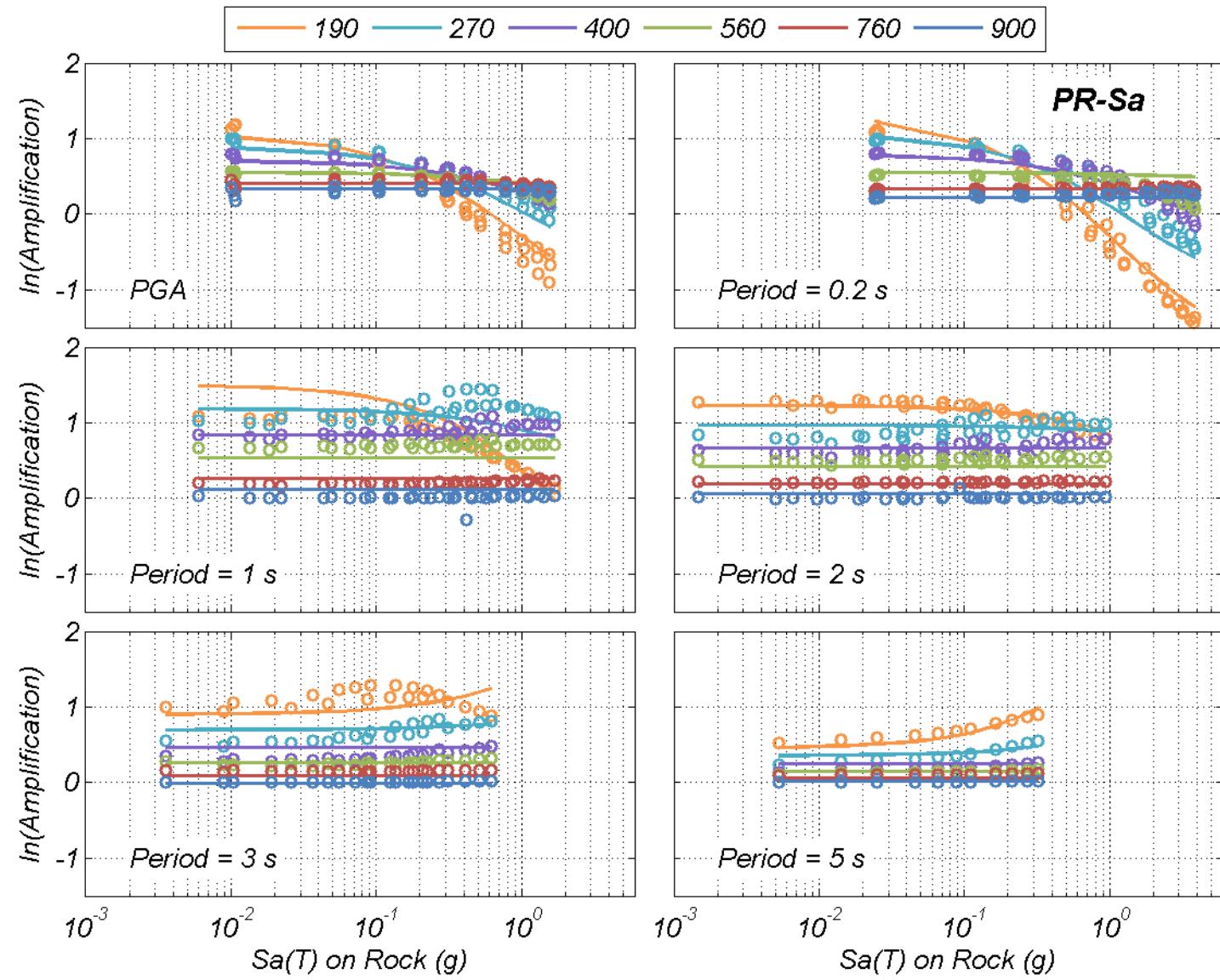
$$\ln(Amp) = \begin{cases} a \ln\left(\frac{V_{s30}^*}{V_{Lin}}\right) - b \ln(PGA_{Rock} + c) \\ + b \ln\left(PGA_{Rock} + c \left(\frac{V_{s30}^*}{V_{Lin}}\right)^n\right) + d & \text{for } V_{s30} < V_{Lin} \\ (a + bn) \ln\left(\frac{V_{s30}^*}{V_{Lin}}\right) + d & \text{for } V_{s30} \geq V_{Lin} \end{cases}$$

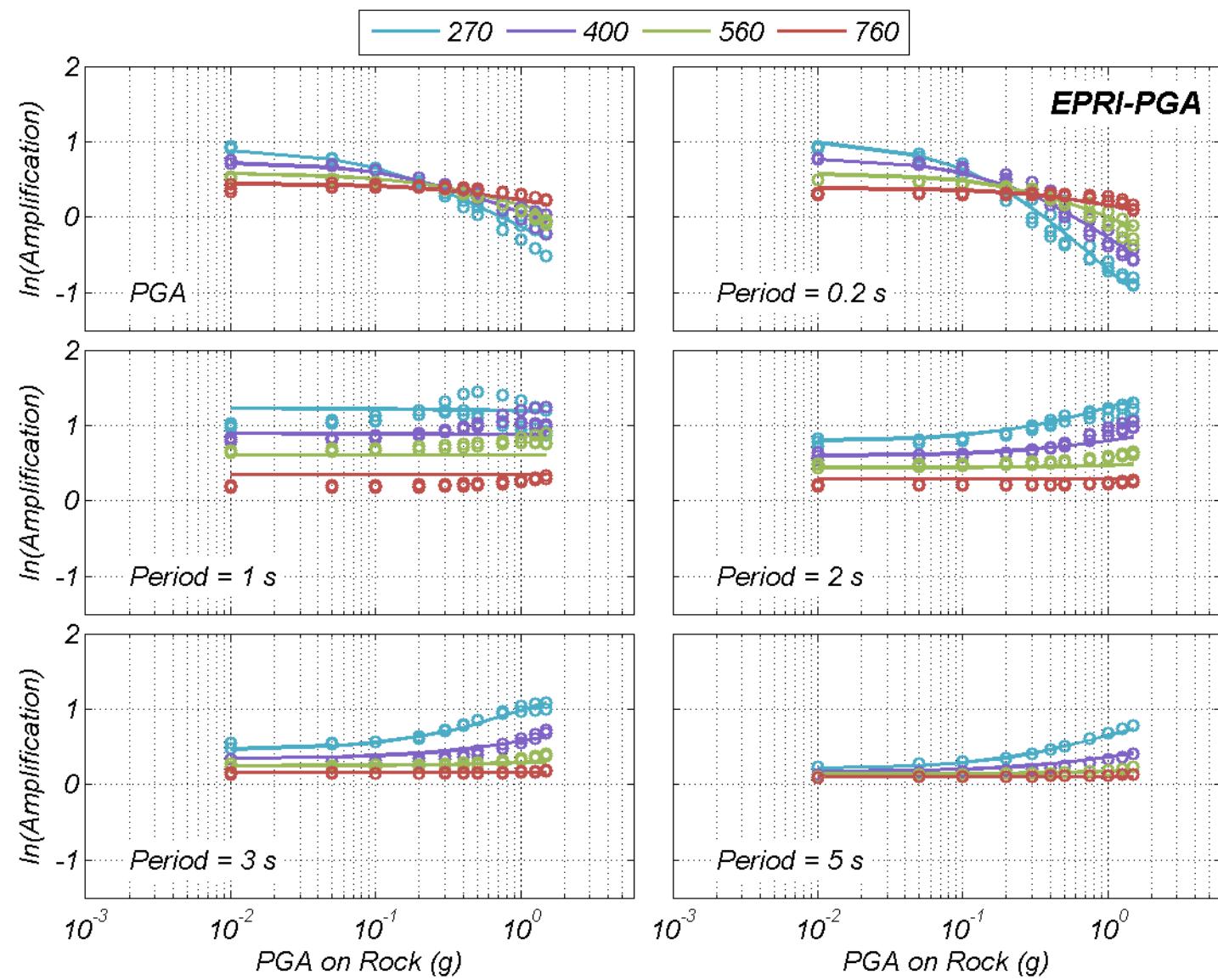
Functional form

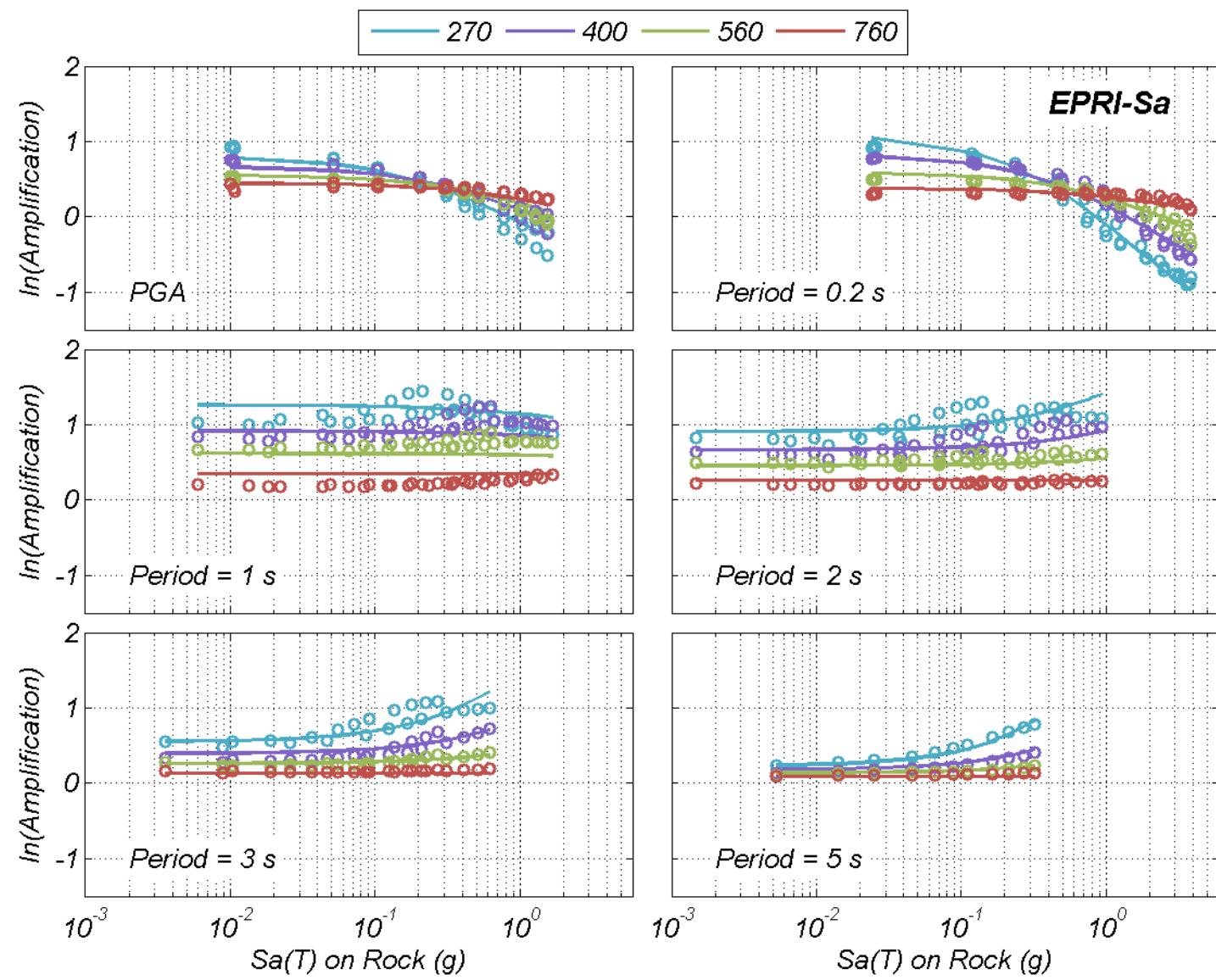
$$\ln(Amp) = f_L(V_{s30}) + f_{NL}(GM_{Rock}, V_{s30})$$

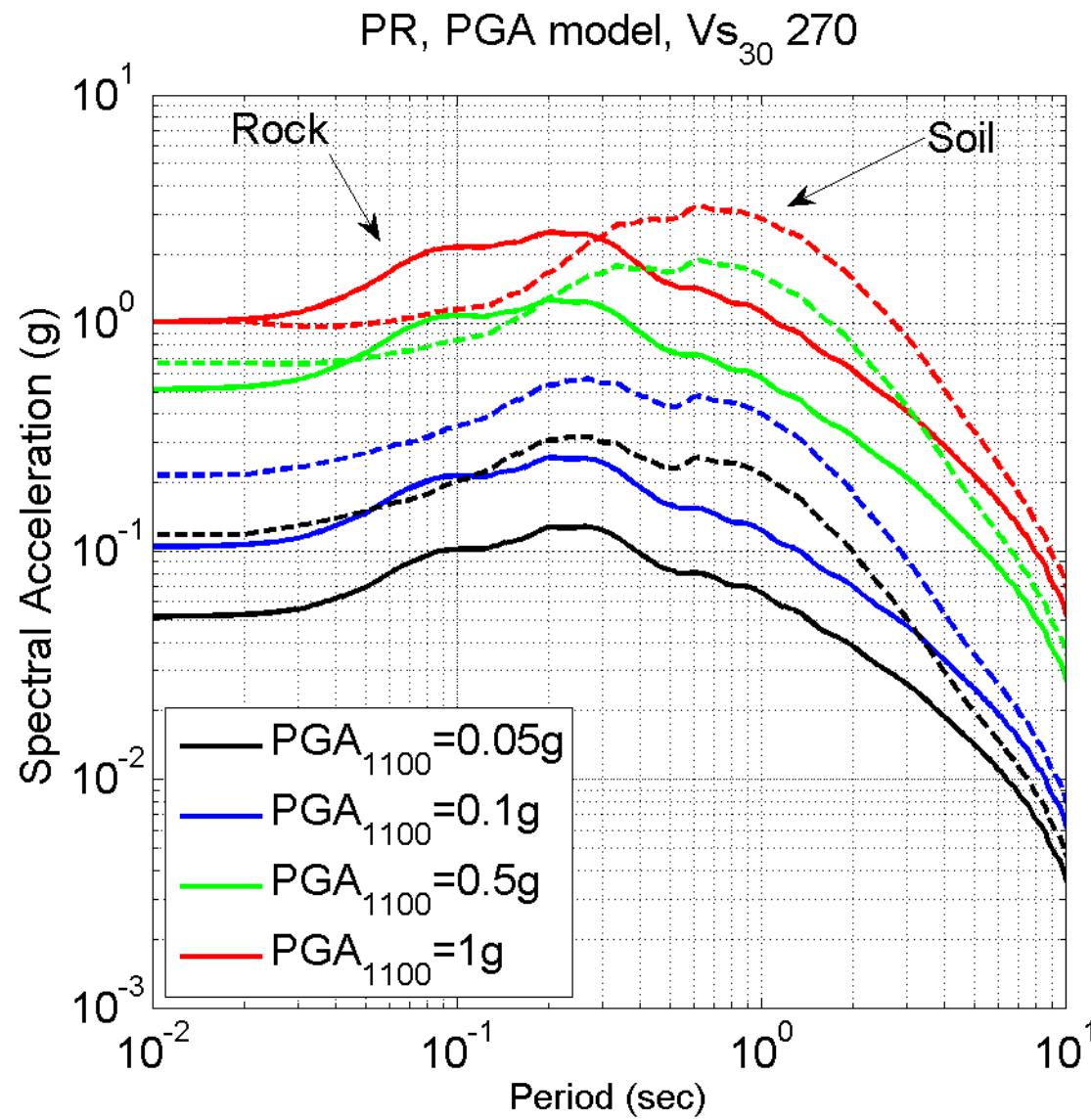
$$\ln(Amp) = \begin{cases} a \ln\left(\frac{V_{s30}^*}{V_{Lin}}\right) - b \ln(S_{aRock}) + c & \\ + b \ln\left(S_{aRock} + c \left(\frac{V_{s30}^*}{V_{Lin}}\right)^n\right) + d & \text{for } V_{s30} < V_{Lin} \\ (a + bn) \ln\left(\frac{V_{s30}^*}{V_{Lin}}\right) + d & \text{for } V_{s30} \geq V_{Lin} \end{cases}$$



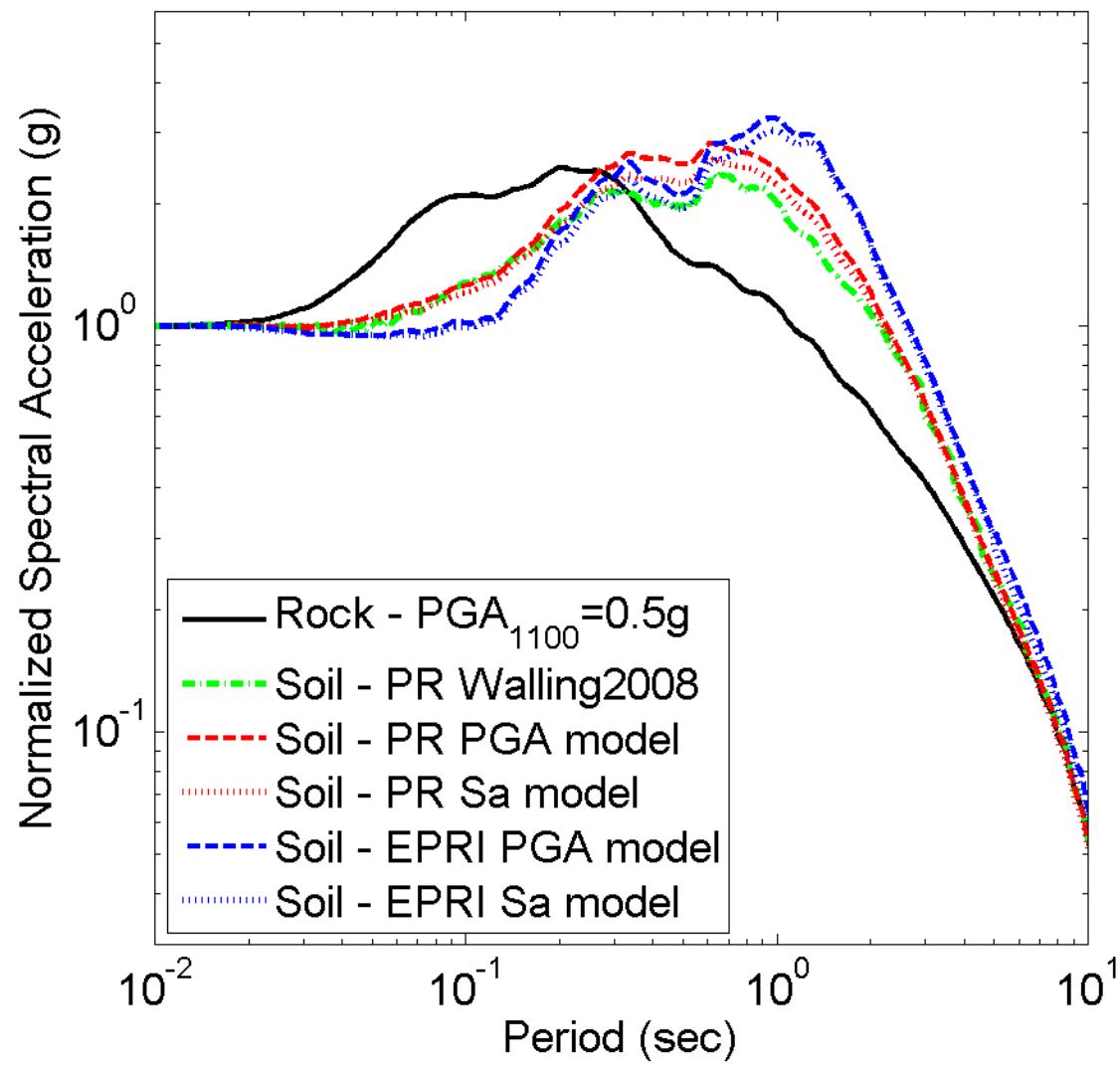




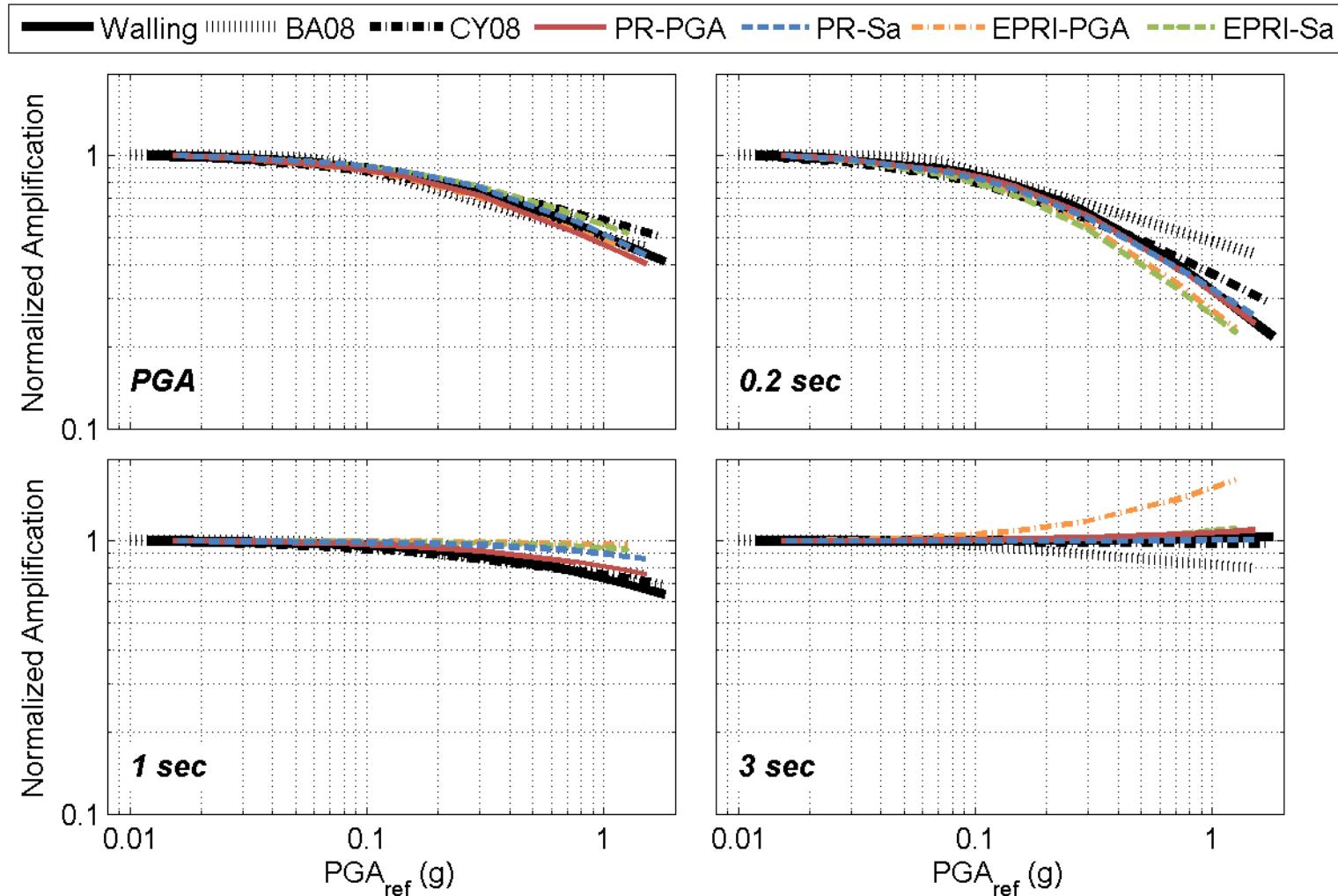




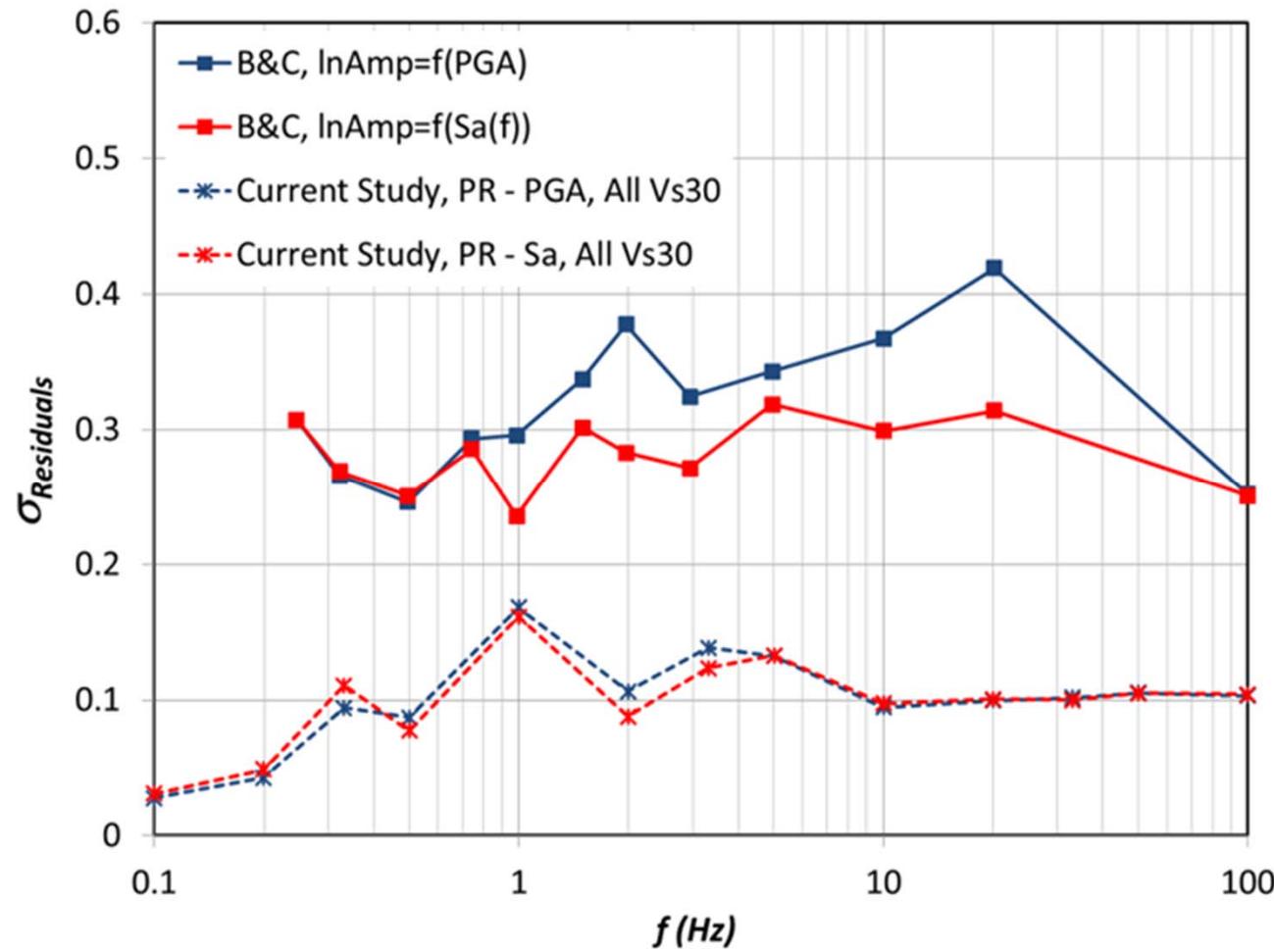
Compare Soil Models, Vs30=270



Nonlinear Soil Amplification for $V_{s30} = 270$, with respect to $V_{s30,ref} = 760 \text{ m/s}$



Should I use PGA or $S_a(T)$ as input motion?



$$b, \ln(V_{Lin}) = \begin{cases} \frac{\beta_2}{\beta_1} & T \geq T_2 \\ \alpha_0 + \sum_{i=1}^8 \alpha_i [\ln(T/T_0)]^i & T_1 < T < T_2 \\ \frac{\beta_1}{\beta_2} & T \leq T_1 \end{cases}$$

	PR PGA Model	PR Sa Model	EPRI PGA Model		EPRI Sa Model	
	V _{LIN}	b	V _{LIN}	b	V _{LIN}	b
T ₀	0.02	0.04	0.02	0.06	0.02	0.04
T ₁	0.02	0.06	0.02	0.082	0.02	0.04
T ₂	0.6	8.8	0.8	5.65	1.1	8.8
α_0	6.514	-1.170	6.554	-1.300	7.093	-0.778
α_1	0.476	-0.018	0.348	0.517	0.064	-0.230
α_2	-0.558	0.126	0.100	-2.469	1.674	1.224
α_3	0.887	0.042	-0.165	3.450	-2.025	-2.722
α_4	-0.662	-0.743	-0.023	-2.800	0.860	1.845
α_5	0.188	0.447	0.024	1.042	-0.159	-0.533
α_6	-0.018	-0.090	-0.003	-0.167	0.011	0.070
α_7	0	0.006	0	0.009	0	-0.004
α_8	0	0	0	0	0	0
β_1	6.514	-1.170	6.554	-1.30	7.093	-0.778
β_2	315.5	0.394	312.0	4.48	610.0	0.411
n	1.5		1.5		1.5	
c	1.4		2.4		2.0	
					3.7	

Summary

- Four models are presented:
 - PR-PGA
 - PR-Sa
 - EPRI-PGA
 - EPRI-Sa
- Sa(T)-based models generally preferred for ease of applicability, although both forms are statistically equivalent
- Nonlinearity generally consistent with Walling2008 and with CY2008

Thank You

rkamai@berkeley.edu



PEER