#### IMPROVED PROCEDURE TO ESTIMATE SEISMIC FORCES IN ANCILLARY SYSTEMS SUPPORTED ON PIERS AND WHARVES: INSPIRATION FROM PROFESSOR CHOPRA

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# **PIERS AND WHARVES**



#### Marine Oil Terminal Plan



Pictures Courtesy William Bruin and Gayle Johnson, SGH

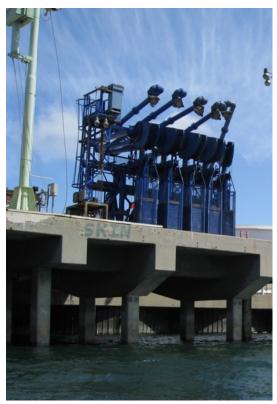
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#### **Marine Oil Terminal Elevation**



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# **ANCILLARY SYSTEMS**









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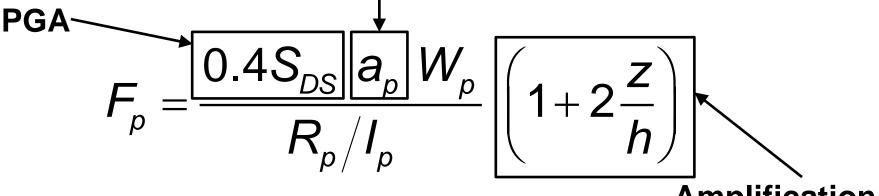
#### **Sign Board**



#### **Hose Cranes**

## **ASCE 7-10 FORMULA**

**Amplification Within Component** 



Amplification Within Structure

 $0.3S_{DS}I_{p}W_{p} < F_{p} < 1.6S_{DS}I_{p}W_{p}$ 

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# **ASCE 7-10 FORMULA**

- $S_{DS}$  = Short period spectral acceleration
  - $a_p =$ Component amplification factor
  - $I_p =$ Component importance factor
  - $R_p$  = Component response modification factor
- $W_{p}$  = Component operating weight
  - z = height in structure of point of attachment of component with respect to base
  - h = average roof height of structure with respect to the base

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# **ASCE 7-10 FORMULA**

- R<sub>p</sub> and a<sub>p</sub> values are provided in tables
- $a_p = 1$  for rigid components;
- $a_p = 2.5$  for flexible components
  - Lower value permitted if justified by detailed dynamic analysis

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# ALTERNATE FORMULA

 If acceleration, a<sub>i</sub>, at the point of attachment of the component can be computed from modal (or response spectrum) method

$$F_{p} = \frac{a_{i}a_{p}W_{p}}{R_{p}/I_{p}}A_{x}$$

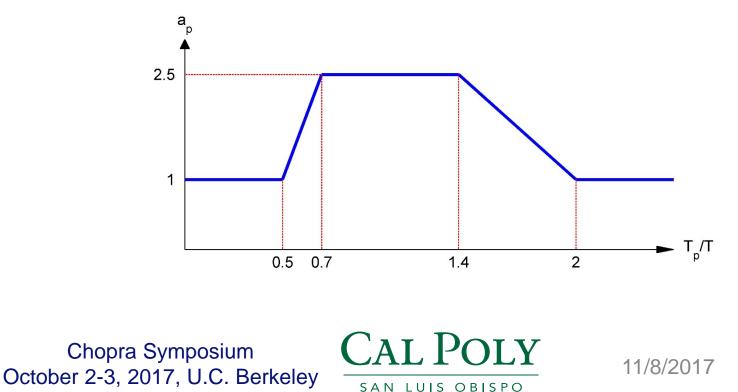
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# ALTERNATE ESTIMATE FOR a<sub>p</sub>

 If fundamental period of the structure, *T*, and of the component, *T<sub>p</sub>*, are know, *a<sub>p</sub>* may be estimated from



### ACCELERATION AT POINT OF ATTACHMENT

- Current Formula
  - Ancillary components are attached at deck level of piers & wharves

$$-z = 1$$
 and  $(1+2z/h) = 3$ 

- Acceleration at point of attachment = 3 times
  PGA
- Independent of primary system period
- Is this appropriate?

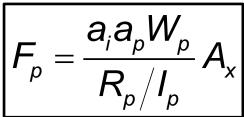
$$F_{p} = \frac{0.4S_{DS} a_{p} W_{p}}{R_{p}/I_{p}} \left(1+2\frac{z}{h}\right)$$

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### ACCELERATION AT POINT OF ATTACHMENT

- Alternate approach to estimating a<sub>i</sub> in piers and wharves
  - Typically one-level structures
  - Most can be idealized as single-degree-offreedom system in direction under consideration
  - a<sub>i</sub> is total acceleration in the SDF system

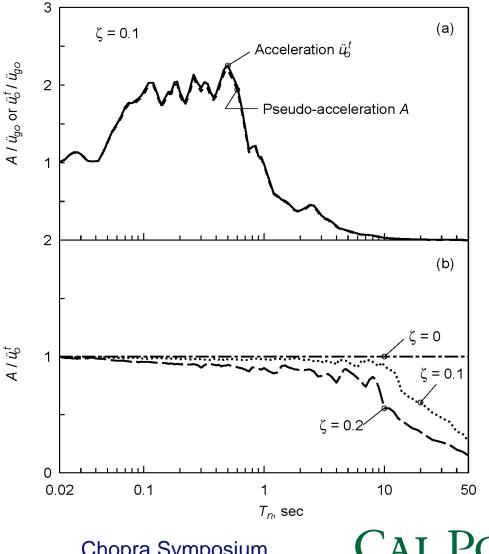


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### **INSPIRATION FROM PROF. CHOPRA**

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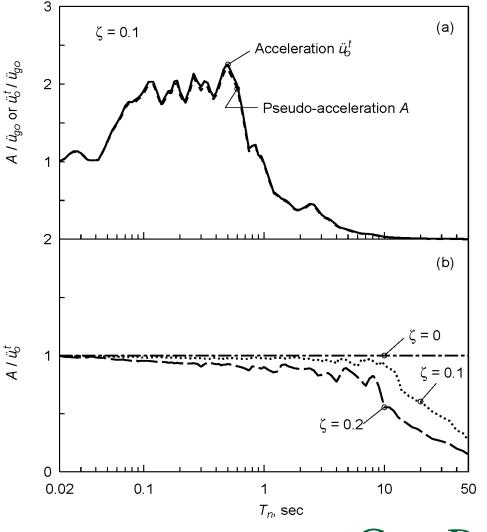


Comparison between pseudo-acceleration (or spectral acceleration) and total acceleration in SDF systems

Figure 6.12.2 from Dynamics of Structures: Theory and Applications to Earthquake Engineering, 5<sup>th</sup> Edition, Anil K. Chopra, PEARSON

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### **INSPIRATION FROM PROF. CHOPRA**



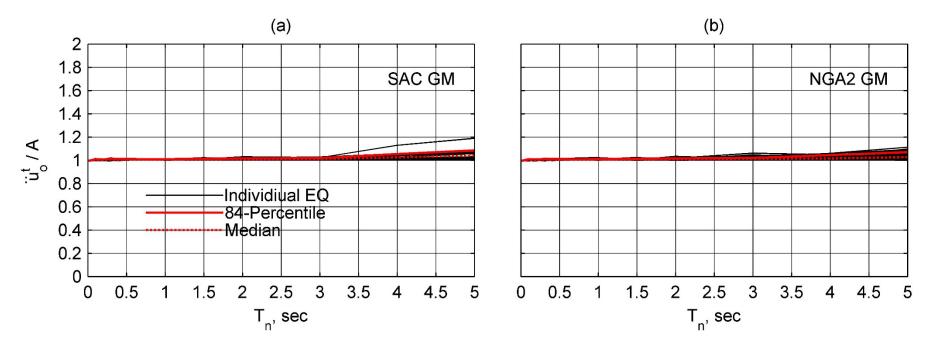
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- Total acceleration and spectral acceleration are theoretically the same for zero damping
- Total acceleration is approximately equal to spectral acceleration for low damping

Figure 6.12.2 from Dynamics of Structures: Theory and Applications to Earthquake Engineering, 5<sup>th</sup> Edition, Anil K. Chopra, PEARSON



## VERIFICATION



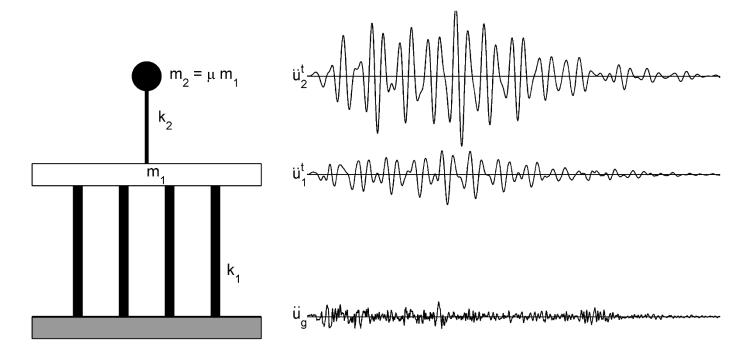
Suite of 20 SAC Ground Motions 5% Damping

Suite of 80 NGA 2 West Ground Motions 5% Damping

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# **AMPLIFICATION FACTOR** a<sub>p</sub>

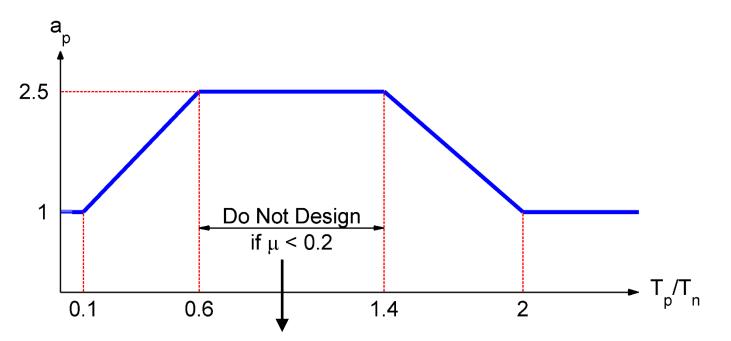


#### A Simple 2 DOF Model to Study Amplification of Acceleration within Component

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### **RECOMMENDATION FOR AMPLIFICATION FACTOR** a<sub>D</sub>



Not permitted because ancillary component will act like tuned-mass damper and will experience excessive motions

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### PROPOSED PROCEDURE FOR PIERS AND WHARVES

ja<sub>p</sub> A

Revised amplification factor

Spectral acceleration at fundamental period of the pier/wharf in direction under consideration

$$0.3S_{DS}I_{\rho}W_{\rho} < F_{\rho} < 1.6S_{DS}I_{\rho}W_{\rho}$$

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#### VERIFICATION **Excellent Estimate Excellent Estimate** 10 10 $T_{\rm p} T_{\rm n} = 0.1$ mu = 0.01 mu = 0.01 mu = 0.1 nu = 0.1 0. <sup>o6</sup>0/<sup>o2</sup>0 <sup>06</sup>0/<sup>07</sup>0 4 10 10 mu = 0.15 mu = 0.2 mu = 0.25 mu = 0.15 mu = 0.2 mu = 0.25 8 8 Recommendation Recommendation 0<sup>6</sup> 0<sup>30</sup> 4 0<sup>6</sup> 0<sup>30</sup> 4 ASCE7-10 Commentary ASCE7-10 Commentar ASCE7-10 Flexible ASCE7-10 Flexible € 84-Percentile € 84-Percentile 0.5 1.5 0.5 1.5 0.5 0.5 0.5 1.5 2 0 2 0 1.5 2 0.5 2 0 1.5 2 0 1 1 0 1 1 T\_ Τ. Т Τ\_ Т Т p/T<sub>n</sub> = 1 mu = 0.01 mu = 0.1 mu**Q** 0.05 Better than ASCE 7-0<sup>6</sup> 0,0<sup>2</sup> 0 10 but not very good estimate for light 10 mu = 0.15 mu = 0.2 mu = 0.25 secondary systems Recommendation 05 0 05 0 00 0 4 ASCE7-10 Commentary with period close to ASCE7-10 Flexible 384-Percentile primary system 0

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í٥

0.5

Т

1.5

2 0

0.5

1.5

2 0

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0.5

1

1.5

2

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 $r_{p}/T_{n} = 2$ 

1.5

2

# SUMMARY

- Inspired by work by Prof. Chopra, a simple procedure has been developed to moreaccurately estimate forces in ancillary components supported on piers and wharves
  - Total acceleration approximated by spectral acceleration
  - Utilizes simplicity of piers and wharves as SDF systems

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