

# Fault Branching

Paul Somerville

URS Pasadena

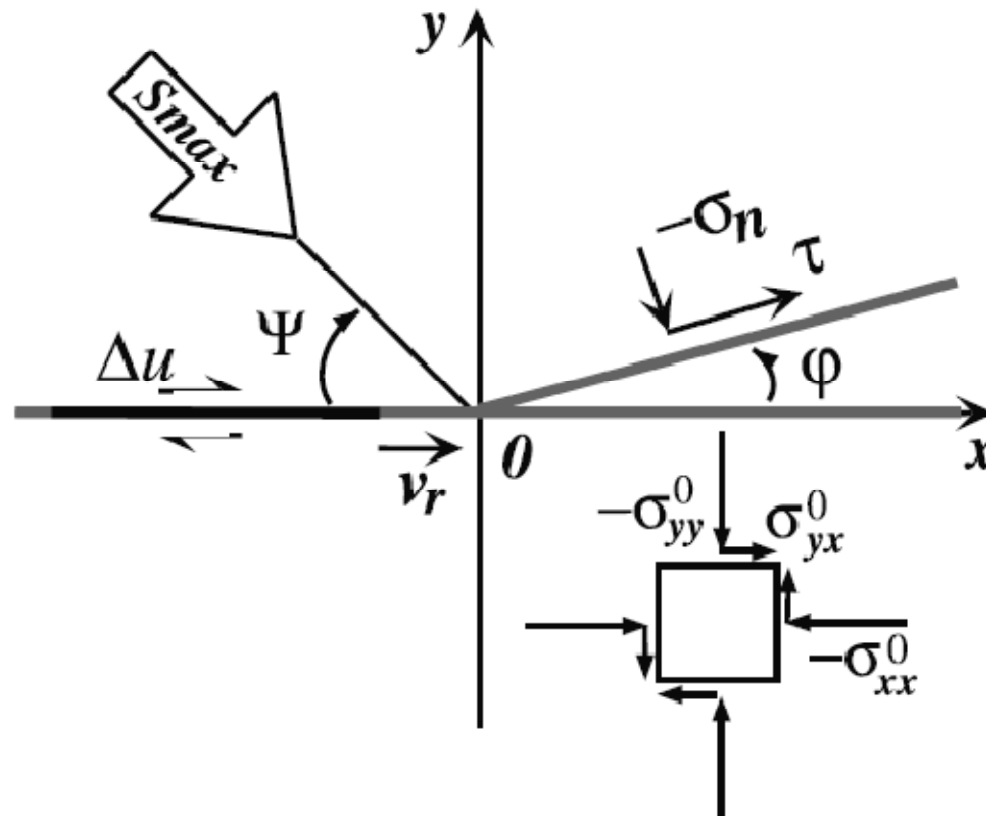
# References – Fault Branching

- Kame, N. and T. Yamashita (1999). Simulation of spontaneous growth of dynamic crack without constraints on the crack tip path. *Geophys. J. Int.* 139, 349-358.
- Kame, N., J.R. Rice and R. Dmowska (2003). Effects of prestress state and rupture velocity on dynamic fault branching. *J. Geophys. Res.* 108, ESE 13-1 – 13-21.

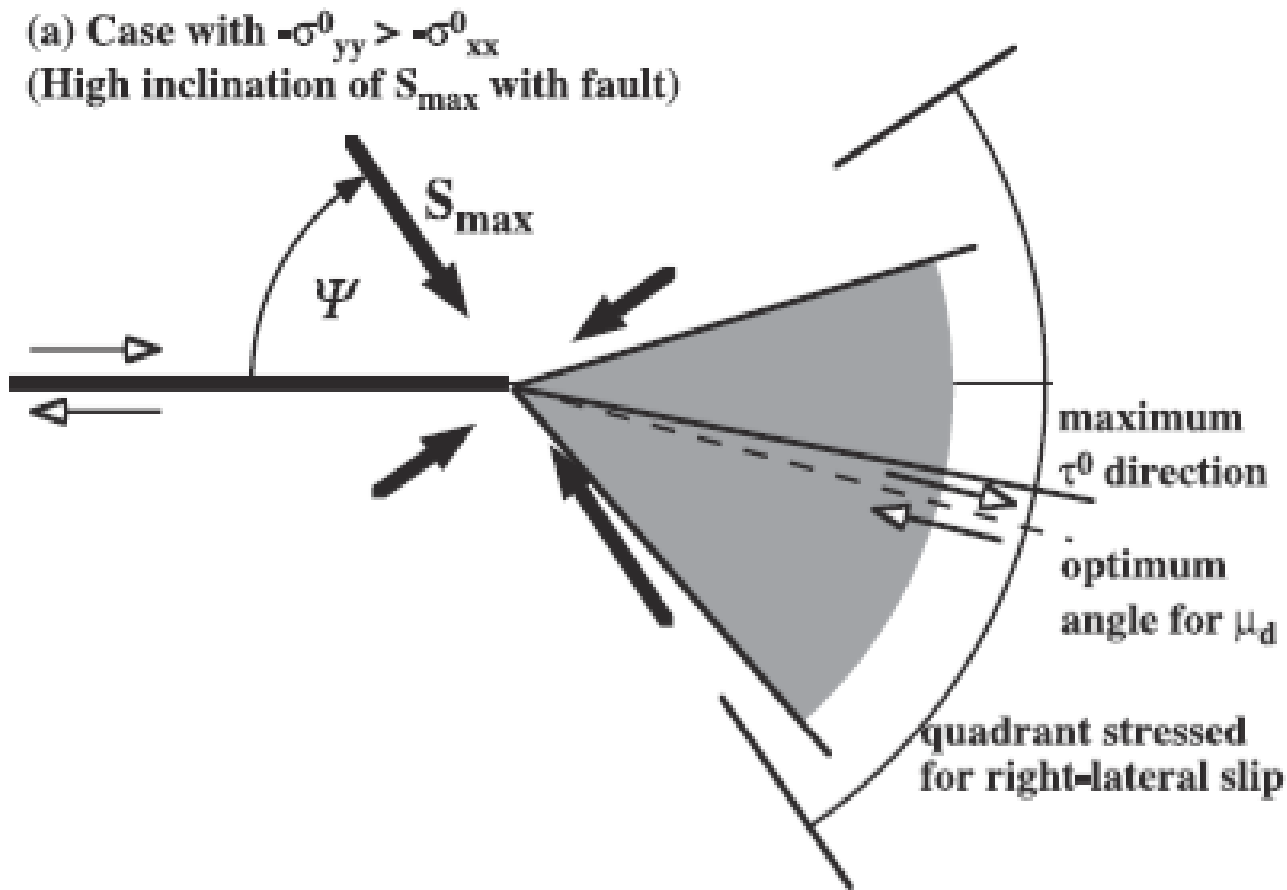
# Fault Branching Model

- Dynamic rupture modeling of strike-slip faulting shows that the rupture prefers to bend than to run straight (Kame and Yamashita, 1999)
- On pre-existing strike-slip faults with branches (Kame et al., 2003), the rupture mode depends on
- $\Psi$  = angle between the direction of maximum compressive stress ( $S_{max}$ ) and the fault strike
- $\phi$  = angle between the main fault and the branch fault
- $v_r$  = rupture velocity (expressed as a fraction of the shear wave velocity  $c_s$ )

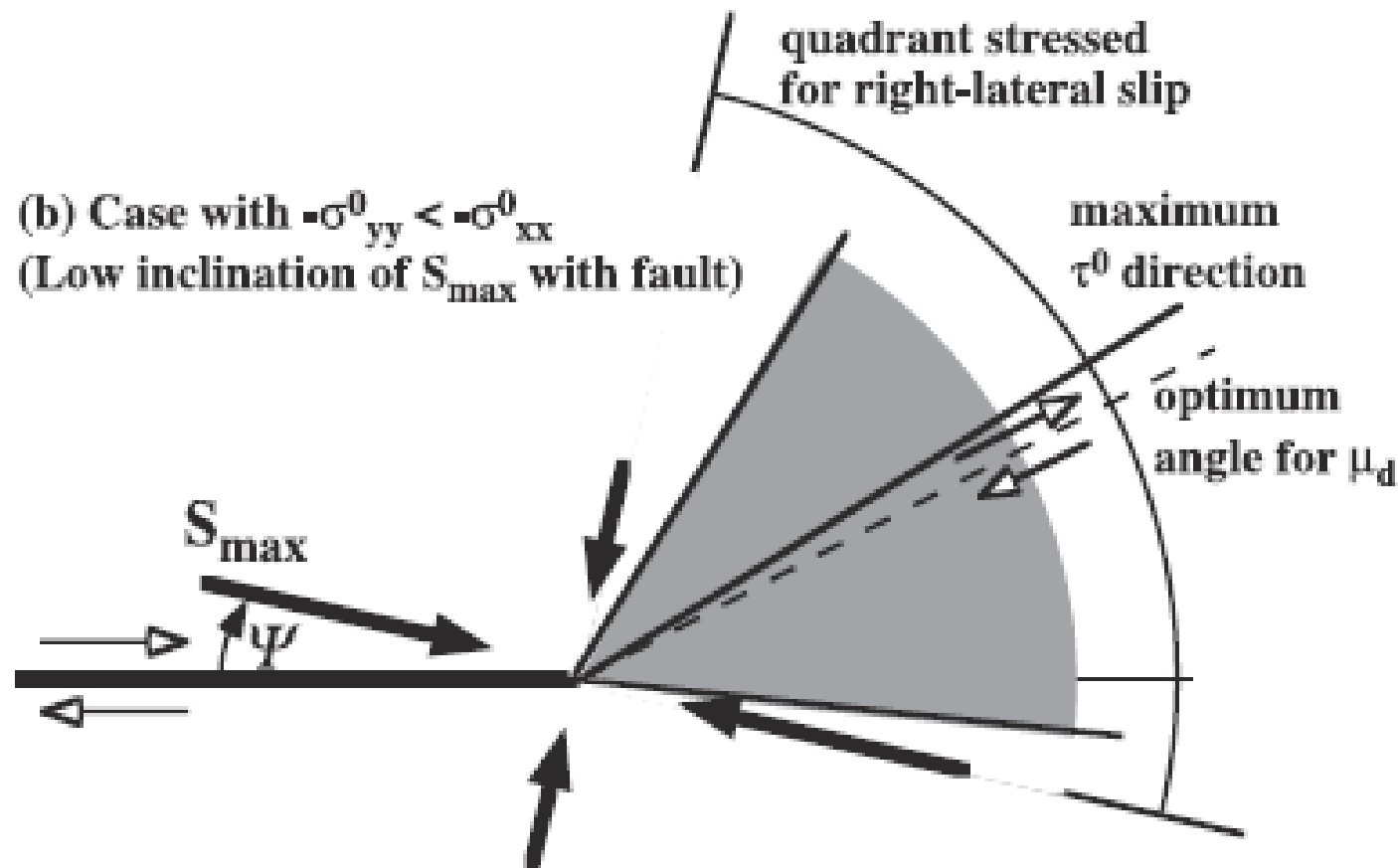
# Configuration of a preexisting branched fault system and prestress state



Fault-normal precompression is dominant,  $\Psi > 45^\circ$ ,  
allowing rupture to continue along bend paths  
primarily to the extensional side



Fault-parallel precompression is dominant,  $\Psi < 45^\circ$ ,  
allowing rupture to continue along bend paths  
primarily to the compressional side



# Rupture Modes

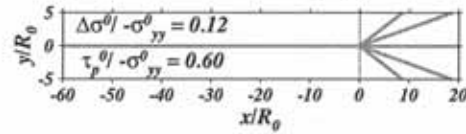
Mode	Description	Examples
1	Rupture on both main fault and branch fault	1979 Imperial Valley 1995 Kobe 1992 Landers
2	Rupture only on branch fault	1990 Luzon 2002 Denali
3	Rupture only on main fault	2001 Kokoxili (Kunlunshan)

# Case Histories of Earthquakes on Branched Faults

EVENT	MAIN FAULT	BRANCH FAULT	REFERENCE
1979 Imperial Valley	<b>Imperial</b>	<b>Brawley</b>	Kame et al., 2003
1990 Luzon	<b>Philippine</b>	<b>Digdig</b>	Rantucci, 1994
1995 Kobe	<b>Suwayama (Gosukebashi)</b>	<b>Okamoto</b>	Sekiguchi et al., 2000
1992 Landers	<b>Johnson</b>	<b>Kickapoo</b>	Kame et al., 2003
2001 Kokoxili (Kunlunshan)	<b>Kunlun</b>	<b>Kitadan</b>	Bhat et al., 2007
2002 Denali	<b>Denali</b>	<b>Totschunda</b>	Bhat et al., 2004



# High Inclination of $S_{\max}$ , $\Psi = 56^\circ$



$$v_r = 0.6 c_s$$

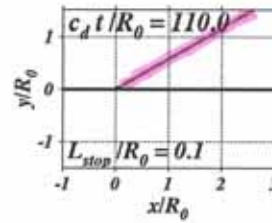
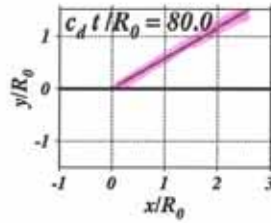
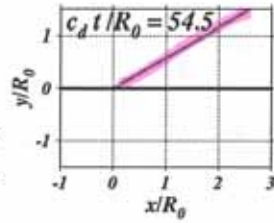
$$v_r = 0.8 c_s$$

$$v_r = 0.9 c_s$$

$$\varphi = +30^\circ$$

$$\Delta\sigma^{\theta}/-\sigma_{yy}^{\theta} = -0.11$$

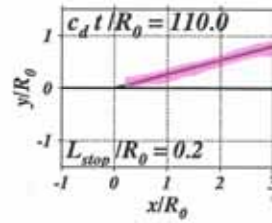
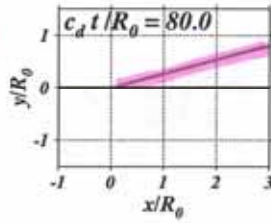
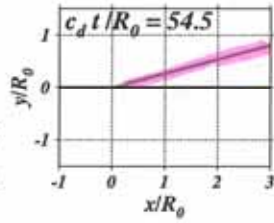
$$\tau_p^{\theta}/-\sigma_{yy}^{\theta} = 0.70$$



$$\varphi = +15^\circ$$

$$\Delta\sigma^{\theta}/-\sigma_{yy}^{\theta} = 0.03$$

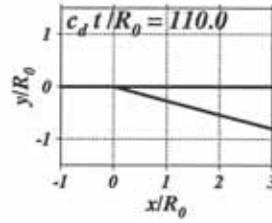
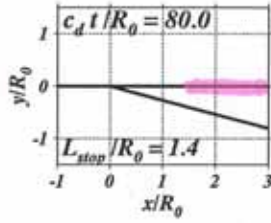
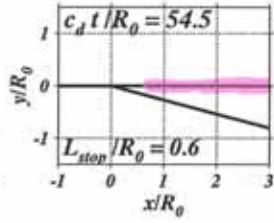
$$\tau_p^{\theta}/-\sigma_{yy}^{\theta} = 0.66$$



$$\varphi = -15^\circ$$

$$\Delta\sigma^{\theta}/-\sigma_{yy}^{\theta} = 0.15$$

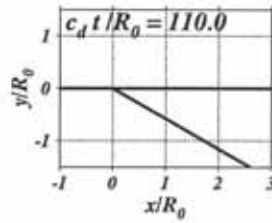
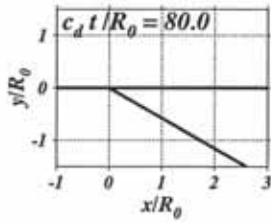
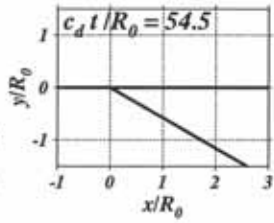
$$\tau_p^{\theta}/-\sigma_{yy}^{\theta} = 0.52$$



$$\varphi = -30^\circ$$

$$\Delta\sigma^{\theta}/-\sigma_{yy}^{\theta} = 0.12$$

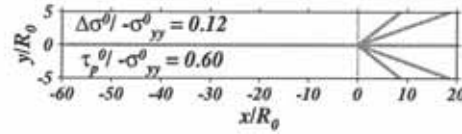
$$\tau_p^{\theta}/-\sigma_{yy}^{\theta} = 0.45$$



2002 Denali

1992 Landers

# Intermediate Inclination of $S_{\max}$ , $\Psi = 45^\circ$



$$v_r = 0.6 c_s$$

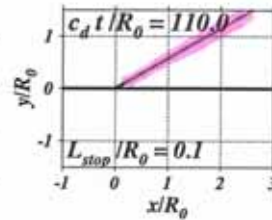
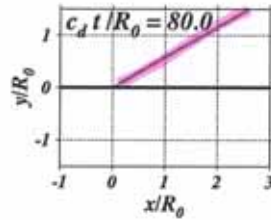
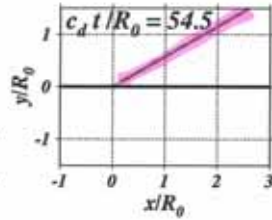
$$v_r = 0.8 c_s$$

$$v_r = 0.9 c_s$$

$$\varphi = +30^\circ$$

$$\Delta\sigma^b / -\sigma_{yy}^0 = -0.03$$

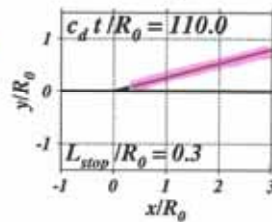
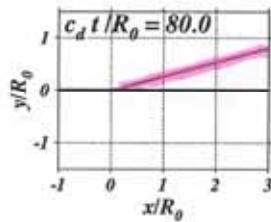
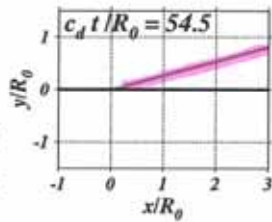
$$\tau_p^b / -\sigma_{yy}^0 = 0.73$$



$$\varphi = +15^\circ$$

$$\Delta\sigma^b / -\sigma_{yy}^0 = 0.07$$

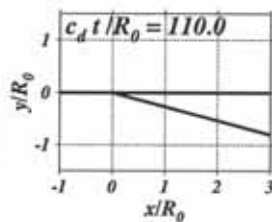
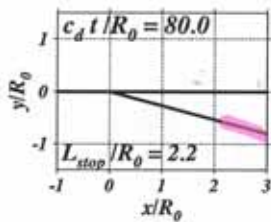
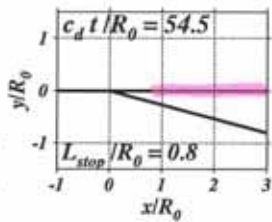
$$\tau_p^b / -\sigma_{yy}^0 = 0.67$$



$$\varphi = -15^\circ$$

$$\Delta\sigma^b / -\sigma_{yy}^0 = 0.10$$

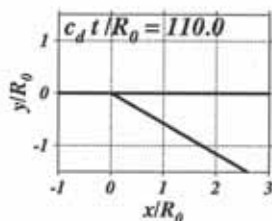
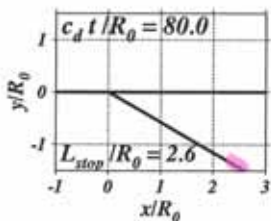
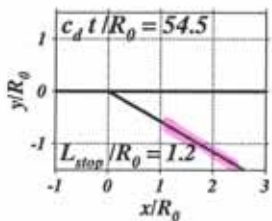
$$\tau_p^b / -\sigma_{yy}^0 = 0.53$$



$$\varphi = -30^\circ$$

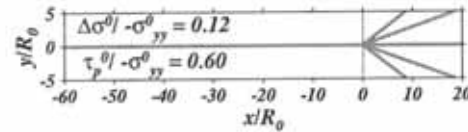
$$\Delta\sigma^b / -\sigma_{yy}^0 = 0.03$$

$$\tau_p^b / -\sigma_{yy}^0 = 0.48$$



1995 Kobe  
 1979 Imperial Valley

# Intermediately Low Inclination of $S_{\max}$ , $\Psi = 25^\circ$



$$v_r = 0.6 c_s$$

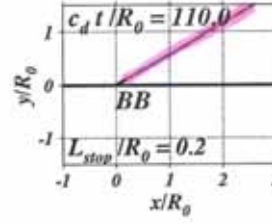
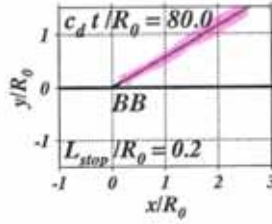
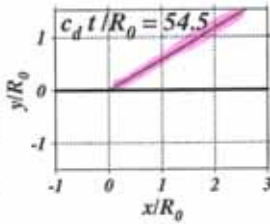
$$v_r = 0.8 c_s$$

$$v_r = 0.9 c_s$$

$$\varphi = +30^\circ$$

$$\Delta\sigma^b/\sigma_{yy}^0 = 0.14$$

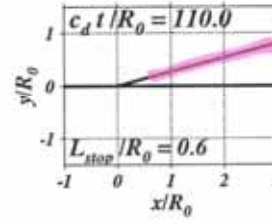
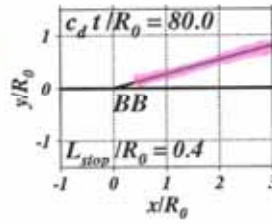
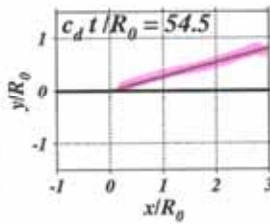
$$\tau_p^b/\sigma_{yy}^0 = 0.79$$



$$\varphi = +15^\circ$$

$$\Delta\sigma^b/\sigma_{yy}^0 = 0.17$$

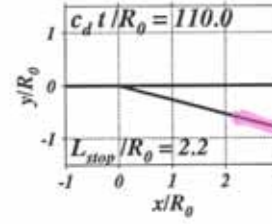
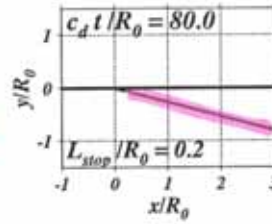
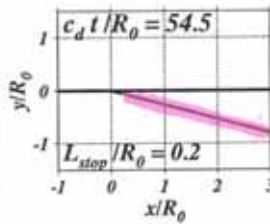
$$\tau_p^b/\sigma_{yy}^0 = 0.69$$



$$\varphi = -15^\circ$$

$$\Delta\sigma^b/\sigma_{yy}^0 = -0.00$$

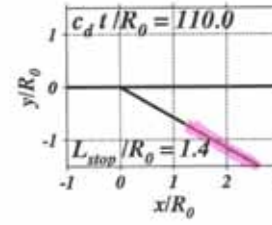
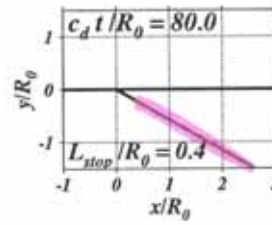
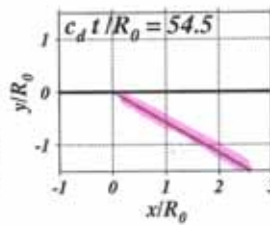
$$\tau_p^b/\sigma_{yy}^0 = 0.54$$



$$\varphi = -30^\circ$$

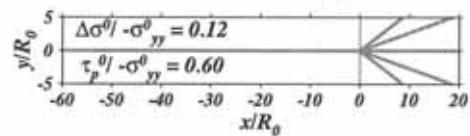
$$\Delta\sigma^b/\sigma_{yy}^0 = -0.16$$

$$\tau_p^b/\sigma_{yy}^0 = 0.54$$



2001 Kokoxili?

Low Inclination of  $S_{\max}$ ,  $\Psi = 13^\circ$

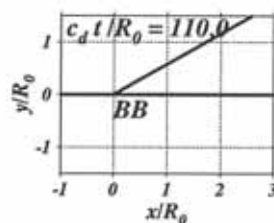
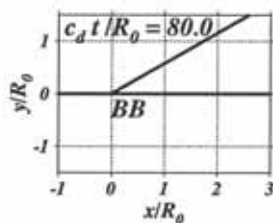
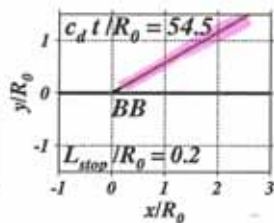


$v_r = 0.6 c_s$

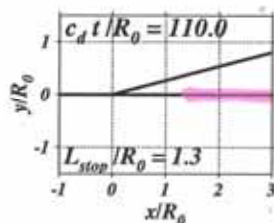
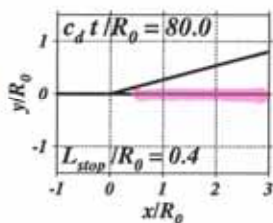
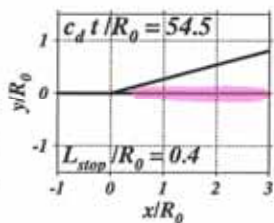
$v_r = 0.8 c_s$

$v_r = 0.9 c_s$

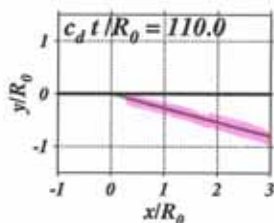
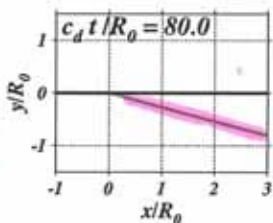
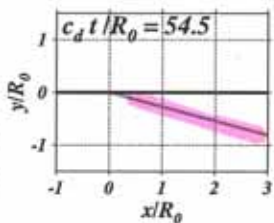
$\varphi = +30^\circ$   
 $\Delta \sigma^b / -\sigma_{yy}^0 = 0.38$   
 $\tau_p^b / -\sigma_{yy}^0 = 0.88$



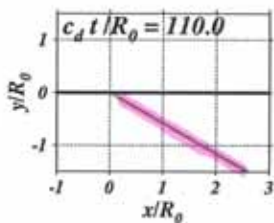
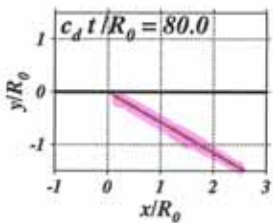
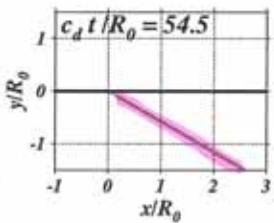
$\varphi = +15^\circ$   
 $\Delta \sigma^b / -\sigma_{yy}^0 = 0.31$   
 $\tau_p^b / -\sigma_{yy}^0 = 0.71$



$\varphi = -15^\circ$   
 $\Delta \sigma^b / -\sigma_{yy}^0 = -0.16$   
 $\tau_p^b / -\sigma_{yy}^0 = 0.57$

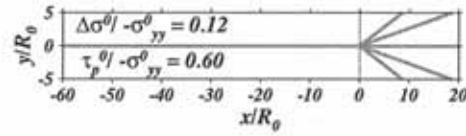


$\varphi = -30^\circ$   
 $\Delta \sigma^b / -\sigma_{yy}^0 = -0.44$   
 $\tau_p^b / -\sigma_{yy}^0 = 0.63$



1990 Luzon?

# High Inclination of $S_{\max}$ , $\Psi = 56^\circ$



$$v_r = 0.6 c_s$$

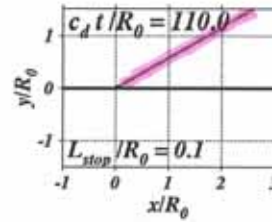
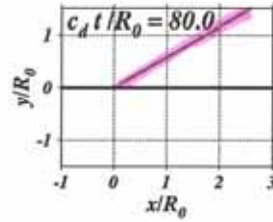
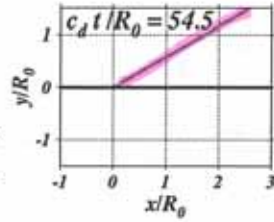
$$v_r = 0.8 c_s$$

$$v_r = 0.9 c_s$$

$$\varphi = +30^\circ$$

$$\Delta \sigma^b / -\sigma_{yy}^b = -0.11$$

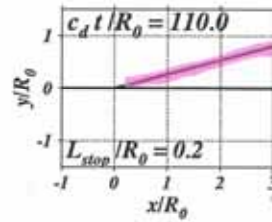
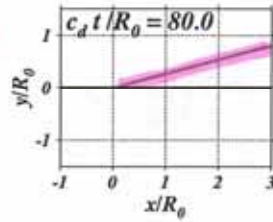
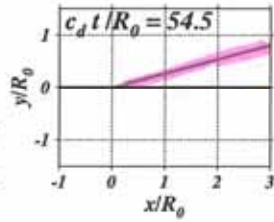
$$\tau_p^b / -\sigma_{yy}^b = 0.70$$



$$\varphi = +15^\circ$$

$$\Delta \sigma^b / -\sigma_{yy}^b = 0.03$$

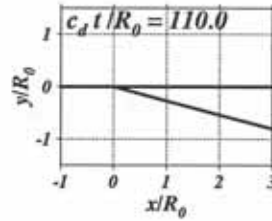
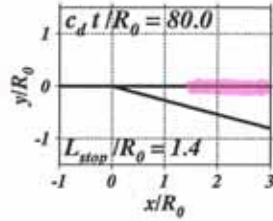
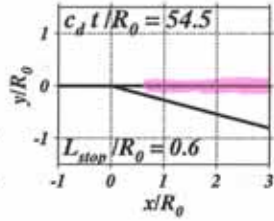
$$\tau_p^b / -\sigma_{yy}^b = 0.66$$



$$\varphi = -15^\circ$$

$$\Delta \sigma^b / -\sigma_{yy}^b = 0.15$$

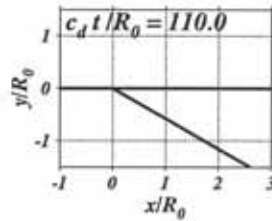
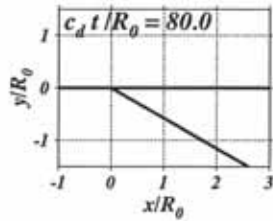
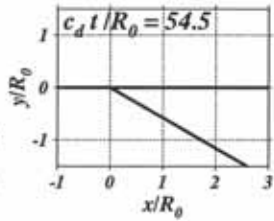
$$\tau_p^b / -\sigma_{yy}^b = 0.52$$



$$\varphi = -30^\circ$$

$$\Delta \sigma^b / -\sigma_{yy}^b = 0.12$$

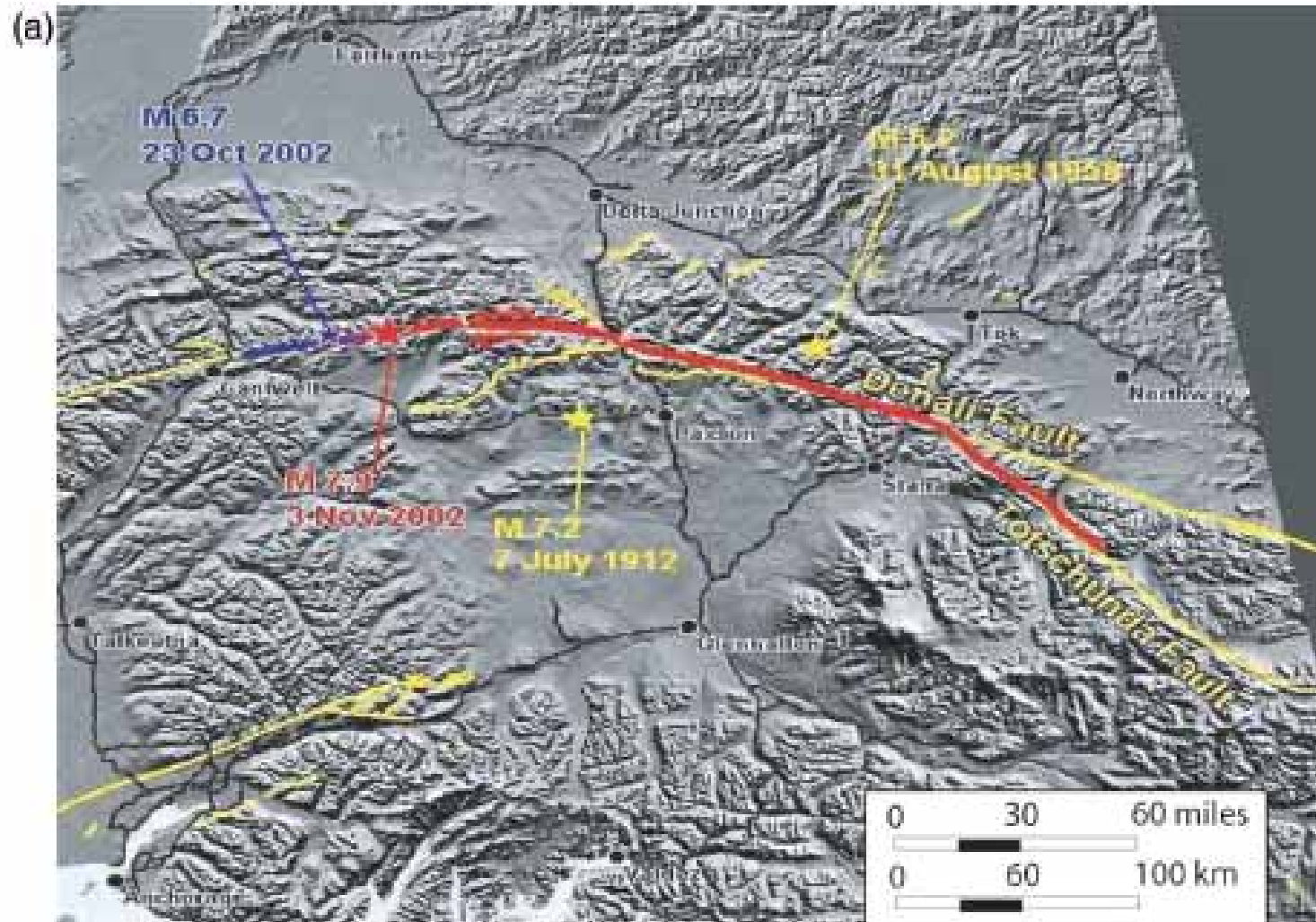
$$\tau_p^b / -\sigma_{yy}^b = 0.45$$



2002 Denali

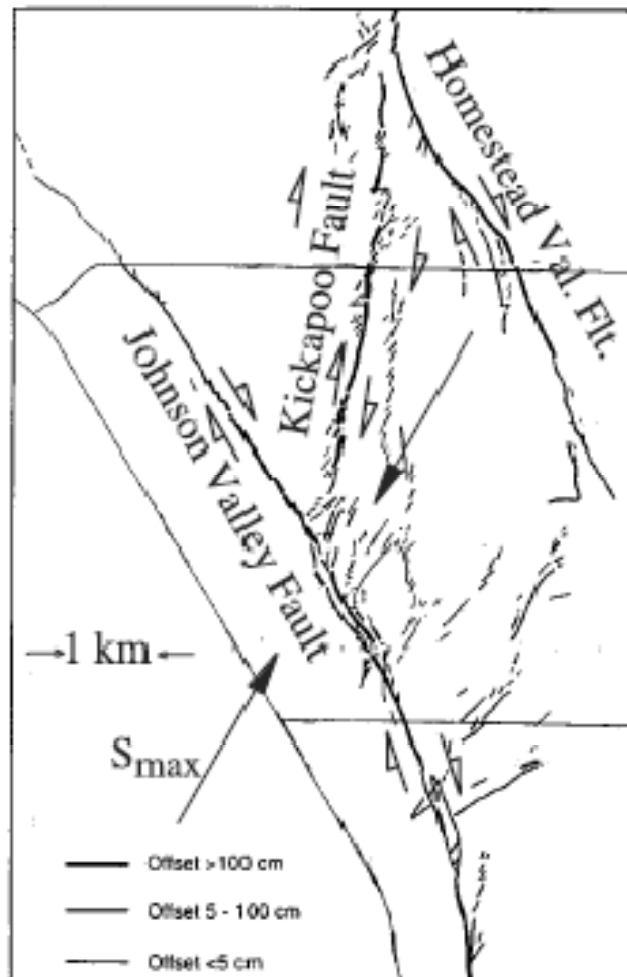
1992 Landers

# Denali



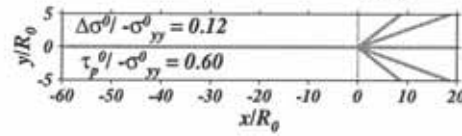
# Landers

Landers 1992





# Intermediate Inclination of $S_{\max}$ , $\Psi = 45^\circ$



$$v_r = 0.6 c_s$$

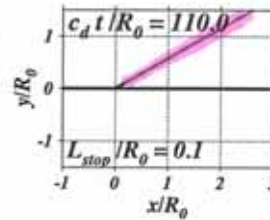
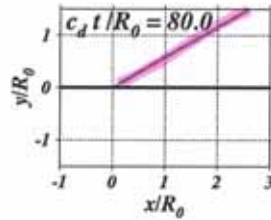
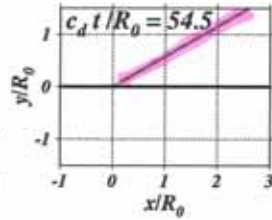
$$v_r = 0.8 c_s$$

$$v_r = 0.9 c_s$$

$$\varphi = +30^\circ$$

$$\Delta\sigma^b / -\sigma_{yy}^0 = -0.03$$

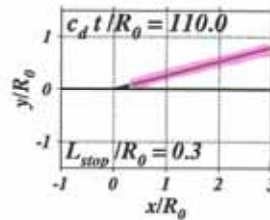
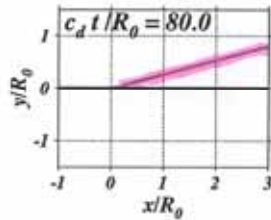
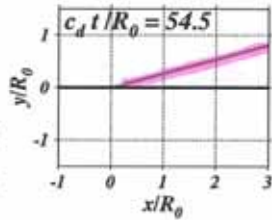
$$\tau_p^b / -\sigma_{yy}^0 = 0.73$$



$$\varphi = +15^\circ$$

$$\Delta\sigma^b / -\sigma_{yy}^0 = 0.07$$

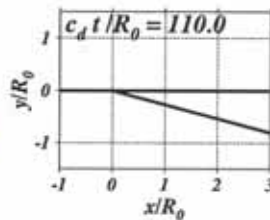
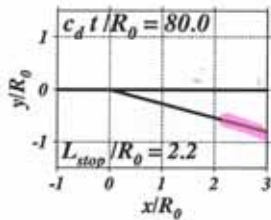
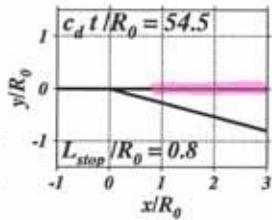
$$\tau_p^b / -\sigma_{yy}^0 = 0.67$$



$$\varphi = -15^\circ$$

$$\Delta\sigma^b / -\sigma_{yy}^0 = 0.10$$

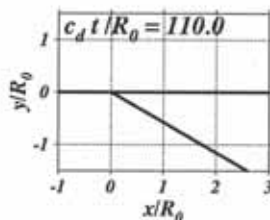
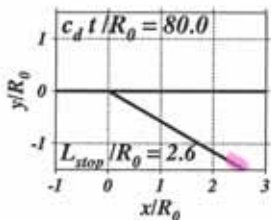
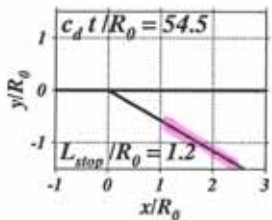
$$\tau_p^b / -\sigma_{yy}^0 = 0.53$$



$$\varphi = -30^\circ$$

$$\Delta\sigma^b / -\sigma_{yy}^0 = 0.03$$

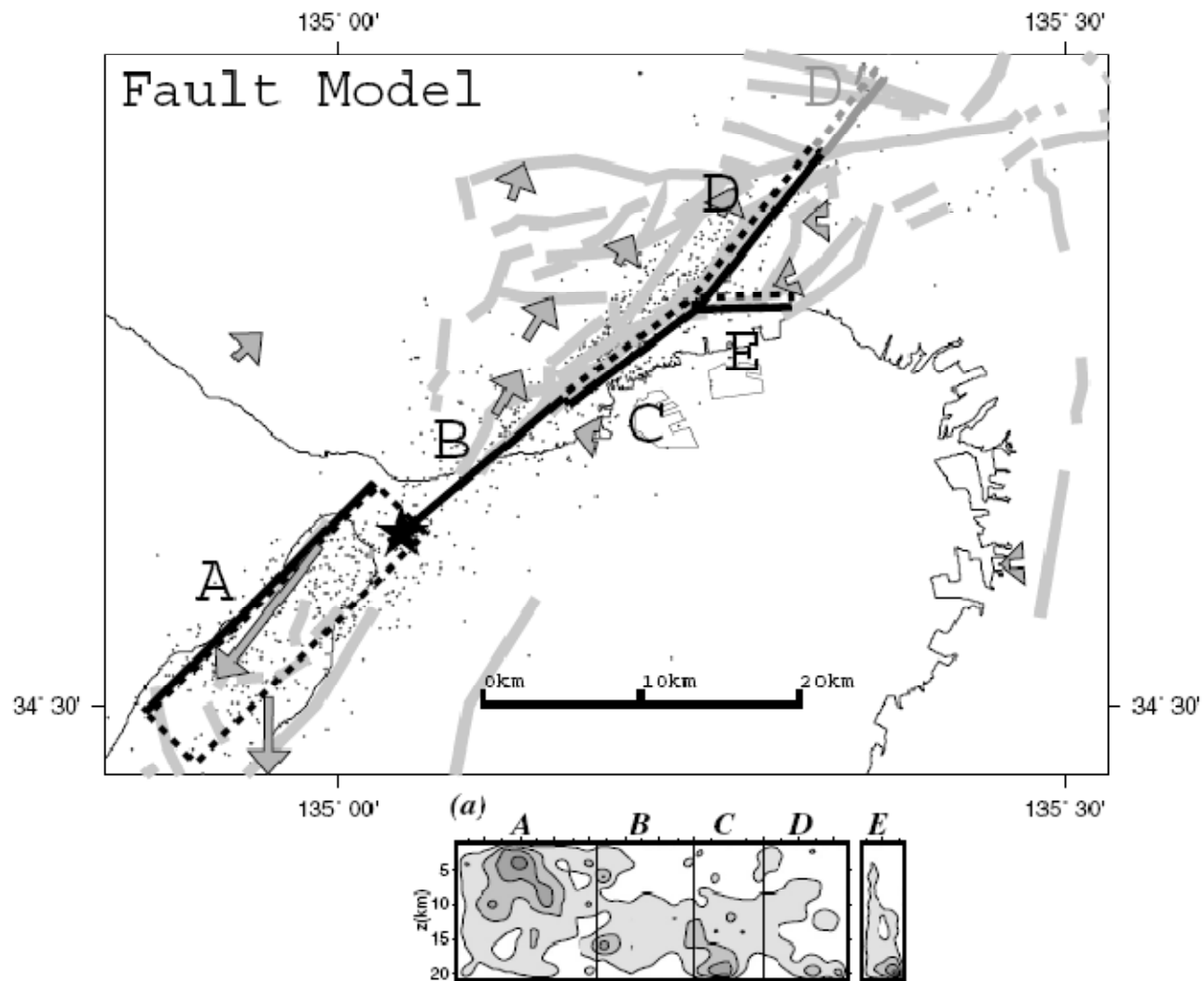
$$\tau_p^b / -\sigma_{yy}^0 = 0.48$$



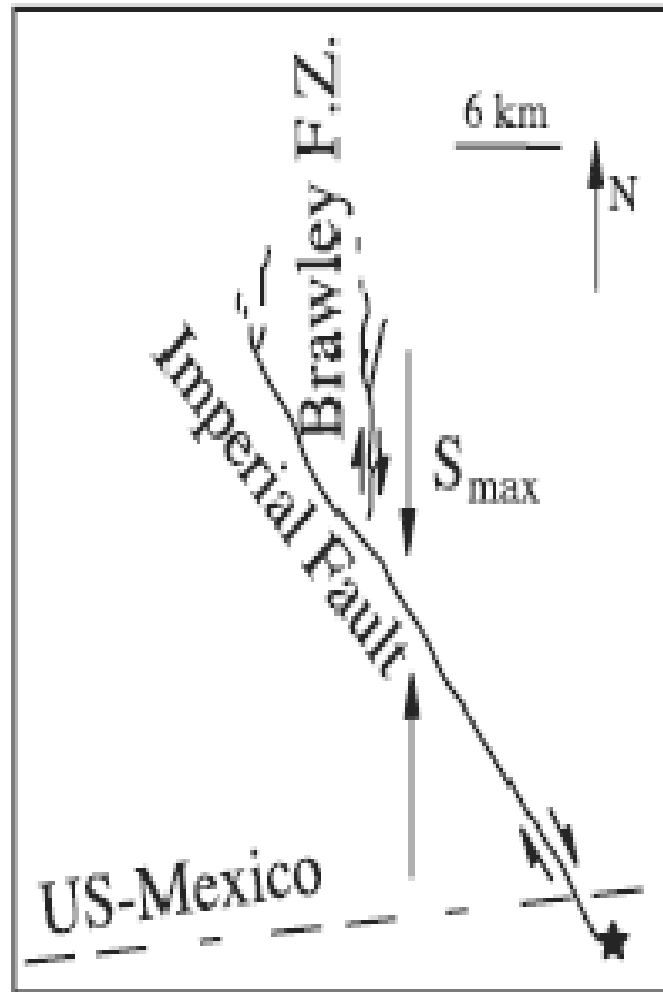
1995 Kobe  
 1979 Imperial Valley



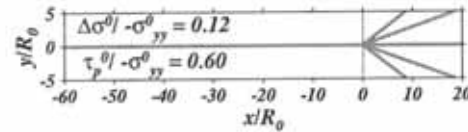
# Kobe



# 1979 Imperial Valley



# Intermediately Low Inclination of $S_{\max}$ , $\Psi = 25^\circ$

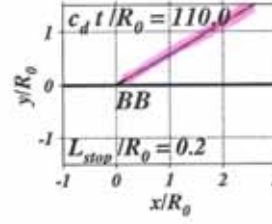
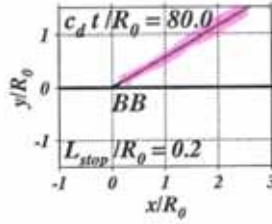
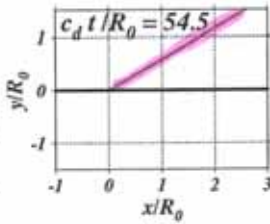


$$v_r = 0.6 c_s$$

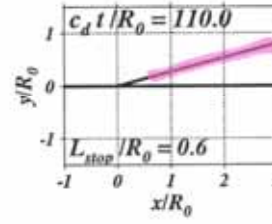
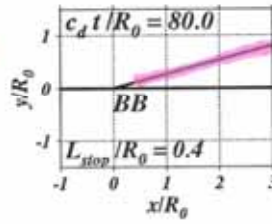
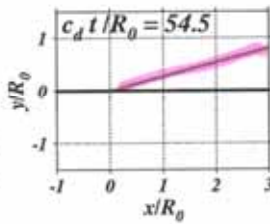
$$v_r = 0.8 c_s$$

$$v_r = 0.9 c_s$$

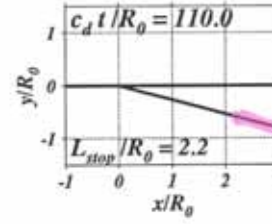
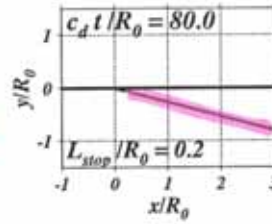
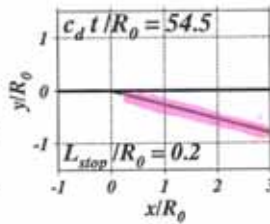
$$\begin{aligned} \varphi &= +30^\circ \\ \Delta\sigma^b/\sigma_{yy}^0 &= 0.14 \\ \tau_p^b/\sigma_{yy}^0 &= 0.79 \end{aligned}$$



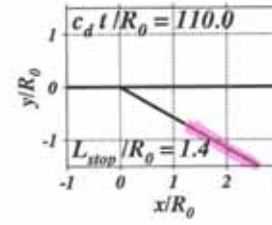
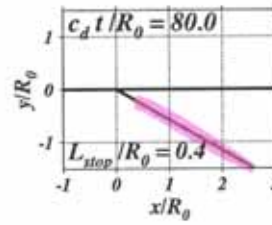
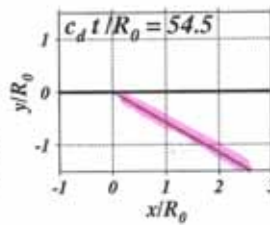
$$\begin{aligned} \varphi &= +15^\circ \\ \Delta\sigma^b/\sigma_{yy}^0 &= 0.17 \\ \tau_p^b/\sigma_{yy}^0 &= 0.69 \end{aligned}$$



$$\begin{aligned} \varphi &= -15^\circ \\ \Delta\sigma^b/\sigma_{yy}^0 &= -0.00 \\ \tau_p^b/\sigma_{yy}^0 &= 0.54 \end{aligned}$$

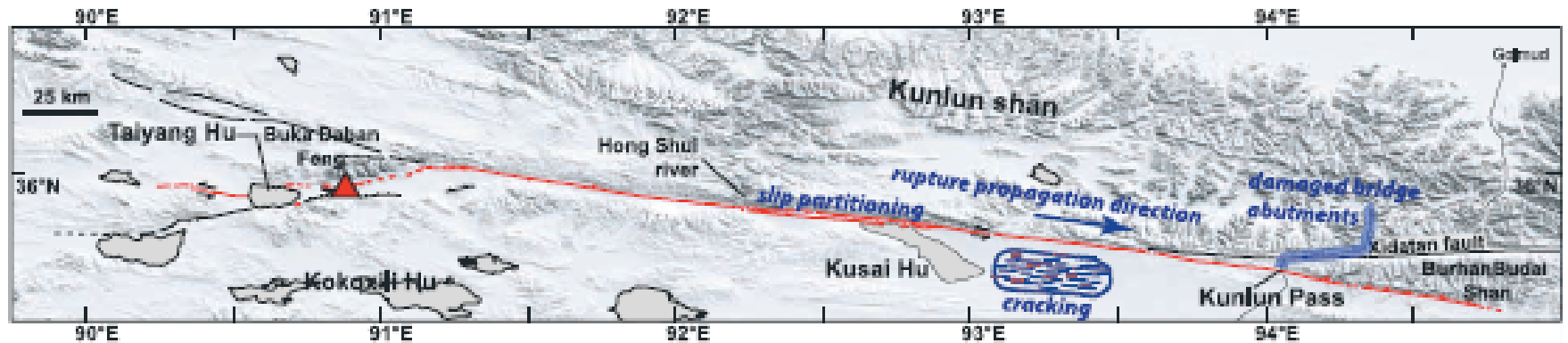


$$\begin{aligned} \varphi &= -30^\circ \\ \Delta\sigma^b/\sigma_{yy}^0 &= -0.16 \\ \tau_p^b/\sigma_{yy}^0 &= 0.54 \end{aligned}$$

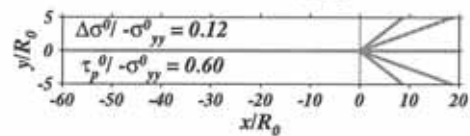


2001 Kokoxili?

# Kokoxili



Low Inclination of  $S_{\max}$ ,  $\Psi = 13^\circ$

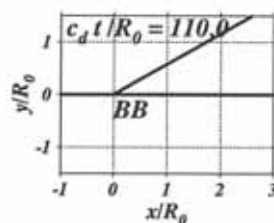
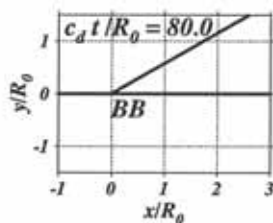
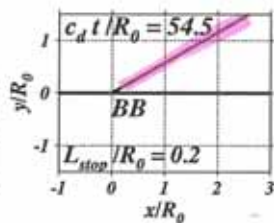


$v_r = 0.6 c_s$

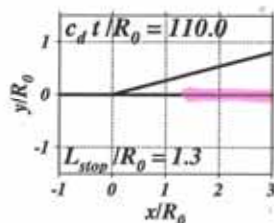
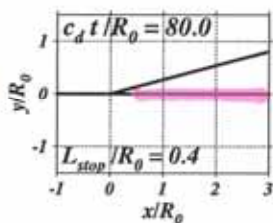
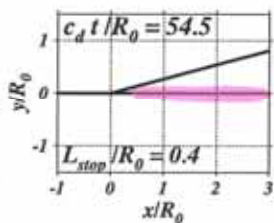
$v_r = 0.8 c_s$

$v_r = 0.9 c_s$

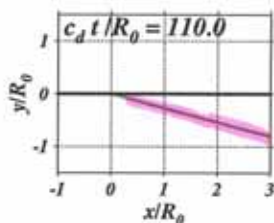
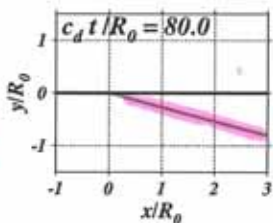
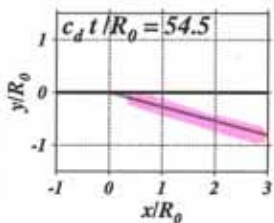
$\varphi = +30^\circ$   
 $\Delta\sigma^b / -\sigma_{yy}^0 = 0.38$   
 $\tau_p^b / -\sigma_{yy}^0 = 0.88$



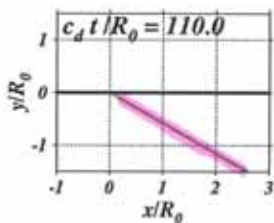
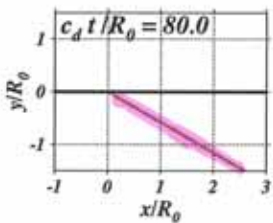
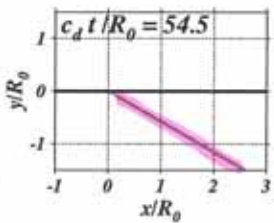
$\varphi = +15^\circ$   
 $\Delta\sigma^b / -\sigma_{yy}^0 = 0.31$   
 $\tau_p^b / -\sigma_{yy}^0 = 0.71$



$\varphi = -15^\circ$   
 $\Delta\sigma^b / -\sigma_{yy}^0 = -0.16$   
 $\tau_p^b / -\sigma_{yy}^0 = 0.57$



$\varphi = -30^\circ$   
 $\Delta\sigma^b / -\sigma_{yy}^0 = -0.44$   
 $\tau_p^b / -\sigma_{yy}^0 = 0.63$



1990 Luzon?

# Luzon

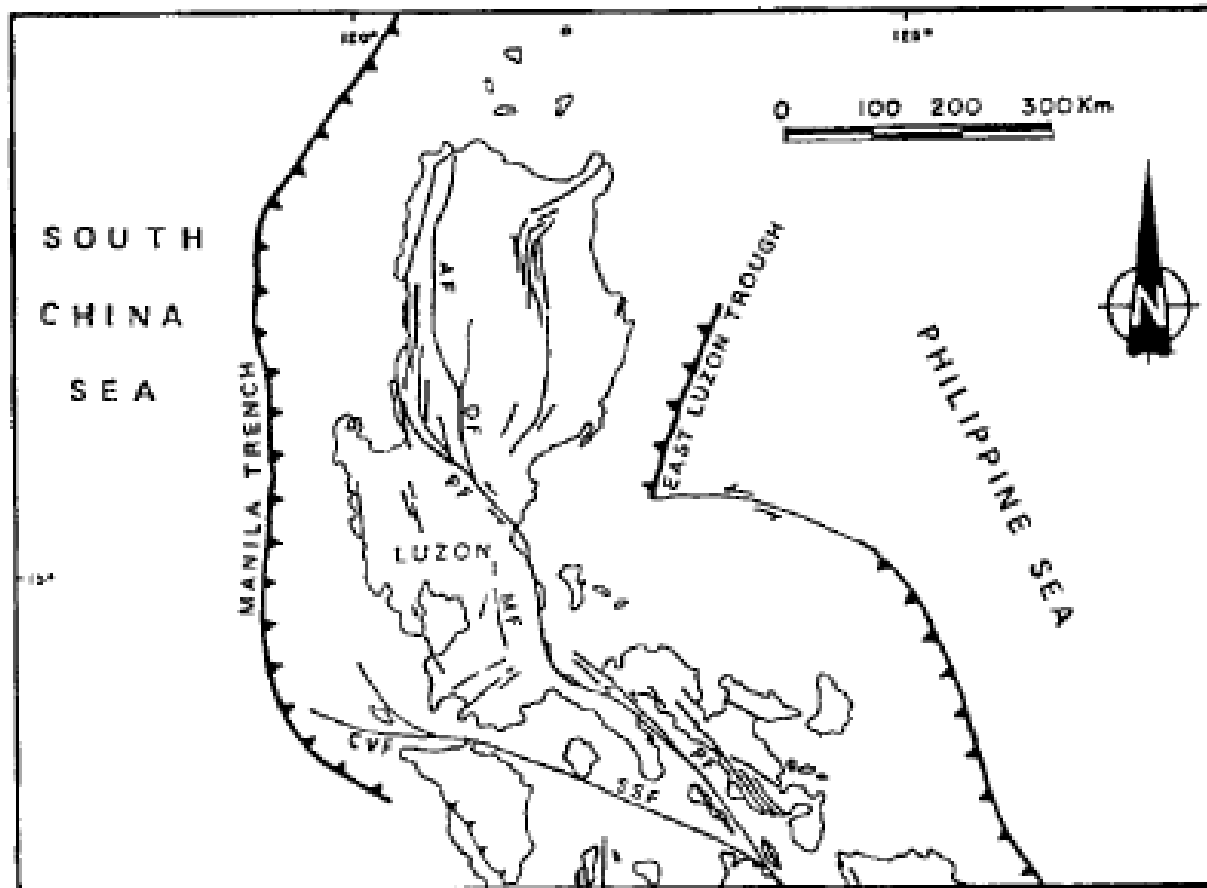


Fig.4.8 - Major tectonic lineaments in Luzon (PF = Philippine Fault, DF = Digdig Fault, AF = Abra Fault, MF = Manila Fault), from Punongbayan and Umbal (1990).

# Luzon

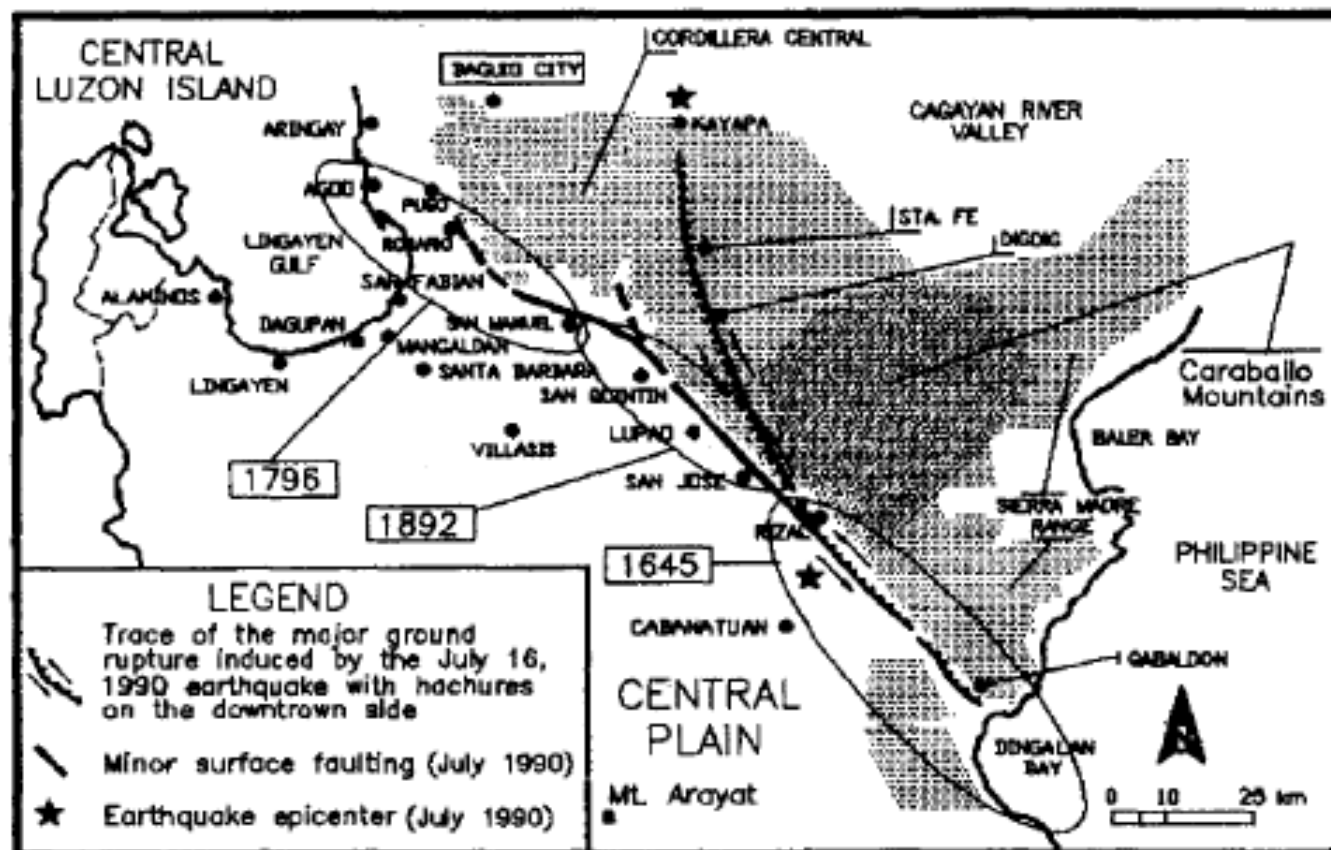


Fig. 4.9 – Location of the Major Ground Rupture and minor surface faultings in Central Luzon associated with the July 1990 earthquake and the areas affected by the 1645, 1796, 1892 earthquakes.

# Conclusions

- We have analyzed six events involving rupture on branched faults which represent three possible modes of fault branching behavior.
- In three cases, including the 1979 Imperial Valley, 1995 Kobe, and 1992 Landers earthquakes, such rupture occurred on both the main fault and the branch fault, all consistent with Kame et al. (2003).
- In the 1990 Luzon and 2002 Denali earthquakes, rupture proceeded onto the branch fault but stopped on the main fault at the branch point.
  - The Denali earthquake observations are consistent with Kame et al.
  - The Luzon earthquake observations are potentially consistent, but the uncertainty in the stress field orientation renders this inconclusive with current data.
- In the 2001 Kokoxili (Kunlunshan) earthquake, the main fault continued to rupture without branching onto the Kitadan fault. The Kokoxili earthquake observations are potentially consistent with Kame et al., but the uncertainty in the stress field orientation renders this inconclusive with current data.